

1     **Properties of Cosmic-Ray Sulfur and Determination of the**  
2 **Composition of Primary Cosmic-Ray Carbon, Neon, Magnesium,**  
3                   **and Sulfur:**

4     **Ten-Year Results from the Alpha Magnetic Spectrometer**  
5                   **- SUPPLEMENTAL MATERIAL -**

6                                   (AMS Collaboration)

7 For references see the main text.

8 *Detector.* — AMS is a general purpose high energy particle physics detector in space. The  
9 layout of the detector is shown in Fig. S1. The key elements are the permanent magnet,  
10 the silicon tracker, four planes of time of flight (TOF) scintillation counters, the array of  
11 anticoincidence counters (ACCs), the transition radiation detector (TRD), the ring imaging  
12 Čerenkov detector (RICH), and the electromagnetic calorimeter (ECAL).

13 The AMS coordinate system is concentric with the magnet. The  $x$  axis is parallel to the  
14 main component of the magnetic field and the  $z$  axis points vertically with  $z = 0$  at the  
15 center of the magnet. The  $(y-z)$  plane is the bending plane.

16 The central field of the magnet is 1.4 kG. Before flight, the field was measured in 120 000  
17 locations to an accuracy of better than 2 G.

18 The tracker has nine layers, the first ( $L1$ ) at the top of the detector, the second ( $L2$ )  
19 just above the magnet, six ( $L3$  to  $L8$ ) within the bore of the magnet, and the last ( $L9$ ) just  
20 above the ECAL.  $L2$  to  $L8$  constitute the inner tracker. Each layer contains double-sided  
21 silicon microstrip detectors, which independently measure the  $x$  and  $y$  coordinates. The  
22 tracker accurately determines the trajectory of cosmic rays by multiple measurements of the  
23 coordinates with a resolution in each layer of  $6.2 \mu\text{m}$  for S nuclei in the bending ( $y$ ) direction,  
24 see Fig. S2. Together, the tracker and the magnet measure the rigidity  $R$  of charged cosmic  
25 rays, with a maximum detectable rigidity of 3.3 TV for S nuclei over the 3 m lever arm from  
26  $L1$  to  $L9$ . Each layer of the tracker provides an independent measurement of the charge  $Z$   
27 with a resolution of  $\sigma_Z/Z = 2.9\%$  for S nuclei. Overall, the inner tracker has a resolution of  
28  $\sigma_Z/Z = 1.1\%$ .

29 As seen from Fig. S1, two of the TOF planes are located above the magnet (upper TOF)  
30 and two planes are below the magnet (lower TOF). The overall velocity ( $\beta = v/c$ ) resolution  
31 has been measured to be  $\sigma(1/\beta) = 0.01$  for S nuclei. This discriminates between upward-  
32 and downward-going particles. The pulse heights of the two upper planes are combined  
33 to provide an independent measurement of the charge with an accuracy  $\sigma_Z/Z = 2\%$ . The  
34 pulse heights from the two lower planes are combined to provide another independent charge  
35 measurement with the same accuracy.

36 Sulfur nuclei traversing AMS were triggered as described in Ref. [23]. The trigger effi-  
37 ciency has been measured to be  $>94\%$  with the uncertainty  $< 1\%$  over the entire rigidity  
38 range.

39 Monte Carlo (MC) simulated events were produced using a dedicated program developed  
40 by the collaboration based on the GEANT4-10.3 package [24]. The program simulates elec-  
41 tromagnetic and hadronic [25] interactions of particles in the material of AMS and generates  
42 detector responses. The digitization of the signals is simulated precisely according to the  
43 measured characteristics of the electronics. The simulated events then undergo the same  
44 reconstruction as used for the data.

45 *Event Selection.* — In the first 10 years AMS has collected  $1.8 \times 10^{11}$  cosmic ray events. The  
46 collection time used in this analysis includes only those seconds during which the detector  
47 was in normal operating conditions and, in addition, AMS was pointing within  $40^\circ$  of the  
48 local zenith and the International Space Station was outside of the South Atlantic Anomaly.  
49 Due to the geomagnetic field, this collection time increases with rigidity, reaching  $2.2 \times 10^8$  s  
50 above 30 GV.

51 Sulfur nuclei are required to be downward going and to have a reconstructed track in the  
52 inner tracker which passes through  $L1$ . In the highest rigidity region,  $R \geq 1.2$  TV, the track  
53 is also required to pass through  $L9$ . Track fitting quality criteria such as a  $\chi^2/\text{d.o.f.} < 10$  in

54 the bending coordinate are applied.

55 Charge measurements on  $L1$ , the upper TOF, the inner tracker, and, for  $R > 1.2$  TV,  
56 the lower TOF and  $L9$  are required to be compatible with charge  $Z = 16$ .

57 The measured rigidity is required to be greater than a factor of 1.2 times the maximum  
58 geomagnetic cutoff within the AMS field of view. The cutoff was calculated by backtrac-  
59 ing [26] from the top of AMS out to 50 Earth's radii using the most recent International  
60 Geomagnetic Reference Field model [27].

TABLE SI: The sulfur flux  $\Phi_S$  as a function of rigidity at the top of AMS in units of  $[\text{m}^2 \cdot \text{sr} \cdot \text{s} \cdot \text{GV}]^{-1}$  including errors due to statistics (stat.); contributions to the systematic error from the trigger, background, and acceptance (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic error.

Rigidity [GV]	$\Phi_S$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$
2.15 – 2.40	( 4.047	0.054	0.198	0.581	0.020	0.614 ) $\times 10^{-2}$
2.40 – 2.67	( 3.867	0.044	0.181	0.331	0.012	0.377 ) $\times 10^{-2}$
2.67 – 2.97	( 3.826	0.038	0.174	0.176	0.006	0.248 ) $\times 10^{-2}$
2.97 – 3.29	( 3.543	0.033	0.157	0.085	0.003	0.179 ) $\times 10^{-2}$
3.29 – 3.64	( 3.176	0.028	0.138	0.044	0.000	0.145 ) $\times 10^{-2}$
3.64 – 4.02	( 2.796	0.024	0.120	0.028	0.001	0.124 ) $\times 10^{-2}$
4.02 – 4.43	( 2.328	0.020	0.099	0.020	0.002	0.101 ) $\times 10^{-2}$
4.43 – 4.88	( 2.011	0.016	0.085	0.015	0.003	0.087 ) $\times 10^{-2}$
4.88 – 5.37	( 1.677	0.013	0.071	0.011	0.003	0.072 ) $\times 10^{-2}$
5.37 – 5.90	( 1.392	0.011	0.059	0.008	0.003	0.059 ) $\times 10^{-2}$
5.90 – 6.47	( 1.187	0.009	0.050	0.006	0.002	0.051 ) $\times 10^{-2}$
6.47 – 7.09	( 9.825	0.074	0.415	0.048	0.022	0.418 ) $\times 10^{-3}$
7.09 – 7.76	( 8.096	0.061	0.342	0.037	0.020	0.344 ) $\times 10^{-3}$
7.76 – 8.48	( 6.771	0.051	0.286	0.029	0.017	0.288 ) $\times 10^{-3}$
8.48 – 9.26	( 5.583	0.043	0.236	0.023	0.015	0.238 ) $\times 10^{-3}$
9.26 – 10.1	( 4.626	0.036	0.196	0.019	0.013	0.197 ) $\times 10^{-3}$
10.1 – 11.0	( 3.828	0.031	0.162	0.015	0.011	0.163 ) $\times 10^{-3}$
11.0 – 12.0	( 3.109	0.027	0.132	0.012	0.009	0.132 ) $\times 10^{-3}$
12.0 – 13.0	( 2.555	0.024	0.108	0.009	0.008	0.109 ) $\times 10^{-3}$
13.0 – 14.1	( 2.075	0.020	0.088	0.007	0.007	0.088 ) $\times 10^{-3}$
14.1 – 15.3	( 1.723	0.017	0.073	0.006	0.006	0.073 ) $\times 10^{-3}$
15.3 – 16.6	( 1.413	0.015	0.060	0.005	0.005	0.060 ) $\times 10^{-3}$
16.6 – 18.0	( 1.121	0.012	0.047	0.004	0.004	0.048 ) $\times 10^{-3}$
18.0 – 19.5	( 9.307	0.106	0.394	0.030	0.033	0.396 ) $\times 10^{-4}$
19.5 – 21.1	( 7.687	0.090	0.325	0.025	0.027	0.327 ) $\times 10^{-4}$
21.1 – 22.8	( 6.122	0.074	0.259	0.020	0.022	0.261 ) $\times 10^{-4}$
22.8 – 24.7	( 5.086	0.061	0.215	0.016	0.019	0.217 ) $\times 10^{-4}$
24.7 – 26.7	( 4.235	0.052	0.179	0.013	0.016	0.181 ) $\times 10^{-4}$
26.7 – 28.8	( 3.462	0.044	0.147	0.011	0.013	0.148 ) $\times 10^{-4}$
28.8 – 33.5	( 2.544	0.025	0.108	0.008	0.010	0.109 ) $\times 10^{-4}$
33.5 – 38.9	( 1.741	0.019	0.074	0.005	0.007	0.075 ) $\times 10^{-4}$
38.9 – 45.1	( 1.211	0.014	0.052	0.004	0.005	0.052 ) $\times 10^{-4}$
45.1 – 52.2	( 8.037	0.110	0.344	0.026	0.034	0.346 ) $\times 10^{-5}$
52.2 – 60.3	( 5.350	0.084	0.230	0.017	0.023	0.231 ) $\times 10^{-5}$
60.3 – 69.7	( 3.673	0.065	0.158	0.012	0.017	0.160 ) $\times 10^{-5}$
69.7 – 80.5	( 2.468	0.050	0.107	0.008	0.012	0.108 ) $\times 10^{-5}$
80.5 – 93.0	( 1.635	0.037	0.071	0.006	0.008	0.072 ) $\times 10^{-5}$

*Table continued*

TABLE SI – (Continued).

Rigidity [GV]	$\Phi_S$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$
93.0 – 108	( 1.122	0.028	0.049	0.004	0.006	0.049 ) $\times 10^{-5}$
108 – 125	( 7.496	0.217	0.328	0.028	0.044	0.333 ) $\times 10^{-6}$
125 – 147	( 4.929	0.155	0.217	0.019	0.031	0.220 ) $\times 10^{-6}$
147 – 175	( 3.071	0.108	0.136	0.013	0.021	0.138 ) $\times 10^{-6}$
175 – 211	( 1.886	0.074	0.084	0.009	0.015	0.086 ) $\times 10^{-6}$
211 – 259	( 1.140	0.050	0.051	0.007	0.010	0.053 ) $\times 10^{-6}$
259 – 330	( 6.417	0.305	0.293	0.048	0.069	0.305 ) $\times 10^{-7}$
330 – 441	( 2.649	0.158	0.123	0.028	0.036	0.131 ) $\times 10^{-7}$
441 – 660	( 1.116	0.074	0.053	0.019	0.021	0.060 ) $\times 10^{-7}$
660 – 1200	( 2.944	0.232	0.146	0.112	0.099	0.209 ) $\times 10^{-8}$
1200 – 3000	( 5.130	1.407	0.319	0.143	0.291	0.455 ) $\times 10^{-9}$

TABLE SII: The O flux  $\Phi_{\text{O}}$  as a function of rigidity at the top of AMS in units of  $[\text{m}^2 \cdot \text{sr} \cdot \text{s} \cdot \text{GV}]^{-1}$  including errors due to statistics (stat.); contributions to the systematic error from the trigger, background, and acceptance (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic error. Note, this Table has 48 bins. Table SVIII shows the same O flux in different binning (66 bins). Please see text for details.

Rigidity [GV]	$\Phi_{\text{O}}$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$	
2.15 – 2.40	( 1.658	0.003	0.052	0.020	0.008	0.057 )	$\times 10^0$
2.40 – 2.67	( 1.524	0.002	0.046	0.015	0.005	0.049 )	$\times 10^0$
2.67 – 2.97	( 1.375	0.002	0.040	0.012	0.002	0.042 )	$\times 10^0$
2.97 – 3.29	( 1.215	0.002	0.034	0.009	0.001	0.035 )	$\times 10^0$
3.29 – 3.64	( 1.057	0.001	0.029	0.007	0.000	0.030 )	$\times 10^0$
3.64 – 4.02	( 9.097	0.012	0.248	0.048	0.005	0.253 )	$\times 10^{-1}$
4.02 – 4.43	( 7.730	0.010	0.209	0.035	0.007	0.212 )	$\times 10^{-1}$
4.43 – 4.88	( 6.546	0.008	0.176	0.025	0.008	0.178 )	$\times 10^{-1}$
4.88 – 5.37	( 5.493	0.007	0.147	0.018	0.009	0.148 )	$\times 10^{-1}$
5.37 – 5.90	( 4.578	0.006	0.122	0.013	0.009	0.123 )	$\times 10^{-1}$
5.90 – 6.47	( 3.809	0.005	0.101	0.010	0.008	0.102 )	$\times 10^{-1}$
6.47 – 7.09	( 3.153	0.004	0.084	0.007	0.007	0.085 )	$\times 10^{-1}$
7.09 – 7.76	( 2.591	0.003	0.069	0.006	0.006	0.070 )	$\times 10^{-1}$
7.76 – 8.48	( 2.134	0.003	0.057	0.004	0.005	0.057 )	$\times 10^{-1}$
8.48 – 9.26	( 1.752	0.002	0.047	0.003	0.005	0.047 )	$\times 10^{-1}$
9.26 – 10.1	( 1.434	0.002	0.038	0.003	0.004	0.039 )	$\times 10^{-1}$
10.1 – 11.0	( 1.173	0.002	0.031	0.002	0.003	0.032 )	$\times 10^{-1}$
11.0 – 12.0	( 9.600	0.013	0.257	0.018	0.029	0.260 )	$\times 10^{-2}$
12.0 – 13.0	( 7.874	0.012	0.211	0.015	0.024	0.213 )	$\times 10^{-2}$
13.0 – 14.1	( 6.465	0.010	0.174	0.013	0.021	0.175 )	$\times 10^{-2}$
14.1 – 15.3	( 5.302	0.009	0.143	0.011	0.017	0.144 )	$\times 10^{-2}$
15.3 – 16.6	( 4.356	0.007	0.117	0.009	0.015	0.119 )	$\times 10^{-2}$
16.6 – 18.0	( 3.562	0.006	0.096	0.008	0.012	0.097 )	$\times 10^{-2}$
18.0 – 19.5	( 2.929	0.005	0.079	0.007	0.010	0.080 )	$\times 10^{-2}$
19.5 – 21.1	( 2.403	0.004	0.065	0.006	0.009	0.066 )	$\times 10^{-2}$
21.1 – 22.8	( 1.975	0.004	0.054	0.005	0.007	0.054 )	$\times 10^{-2}$
22.8 – 24.7	( 1.611	0.003	0.044	0.004	0.006	0.044 )	$\times 10^{-2}$
24.7 – 26.7	( 1.316	0.003	0.036	0.004	0.005	0.036 )	$\times 10^{-2}$
26.7 – 28.8	( 1.078	0.002	0.029	0.003	0.004	0.030 )	$\times 10^{-2}$
28.8 – 33.5	( 8.107	0.012	0.222	0.026	0.031	0.225 )	$\times 10^{-3}$
33.5 – 38.9	( 5.477	0.009	0.151	0.019	0.022	0.153 )	$\times 10^{-3}$
38.9 – 45.1	( 3.692	0.007	0.102	0.014	0.015	0.104 )	$\times 10^{-3}$
45.1 – 52.2	( 2.518	0.005	0.070	0.010	0.011	0.072 )	$\times 10^{-3}$
52.2 – 60.3	( 1.712	0.004	0.048	0.008	0.007	0.049 )	$\times 10^{-3}$
60.3 – 69.7	( 1.158	0.003	0.033	0.005	0.005	0.034 )	$\times 10^{-3}$
69.7 – 80.5	( 7.799	0.024	0.223	0.039	0.037	0.229 )	$\times 10^{-4}$

*Table continued*

TABLE SII – (Continued).

Rigidity [GV]	$\Phi_{\text{O}}$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$
80.5 – 93.0	( 5.298	0.019	0.153	0.027	0.026	0.158 ) $\times 10^{-4}$
93.0 – 108	( 3.556	0.014	0.104	0.019	0.019	0.107 ) $\times 10^{-4}$
108 – 125	( 2.390	0.011	0.071	0.013	0.013	0.073 ) $\times 10^{-4}$
125 – 147	( 1.571	0.008	0.047	0.009	0.009	0.049 ) $\times 10^{-4}$
147 – 175	( 9.878	0.053	0.300	0.060	0.064	0.313 ) $\times 10^{-5}$
175 – 211	( 6.145	0.037	0.190	0.041	0.045	0.200 ) $\times 10^{-5}$
211 – 259	( 3.624	0.025	0.114	0.027	0.031	0.122 ) $\times 10^{-5}$
259 – 330	( 1.996	0.015	0.065	0.018	0.021	0.070 ) $\times 10^{-5}$
330 – 441	( 9.834	0.083	0.329	0.120	0.134	0.375 ) $\times 10^{-6}$
441 – 660	( 3.884	0.037	0.136	0.071	0.079	0.173 ) $\times 10^{-6}$
660 – 1200	( 1.086	0.012	0.041	0.036	0.039	0.067 ) $\times 10^{-6}$
1200 – 3000	( 1.502	0.061	0.072	0.052	0.076	0.117 ) $\times 10^{-7}$

TABLE III: The Ne flux  $\Phi_{\text{Ne}}$  as a function of rigidity at the top of AMS in units of  $[\text{m}^2 \cdot \text{sr} \cdot \text{s} \cdot \text{GV}]^{-1}$  including errors due to statistics (stat.); contributions to the systematic error from the trigger, background, and acceptance (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic error.

Rigidity [GV]	$\Phi_{\text{Ne}}$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$
2.15 – 2.40	( 2.552	0.012	0.101	0.056	0.012	0.117 ) $\times 10^{-1}$
2.40 – 2.67	( 2.364	0.010	0.090	0.031	0.007	0.096 ) $\times 10^{-1}$
2.67 – 2.97	( 2.130	0.009	0.079	0.020	0.004	0.082 ) $\times 10^{-1}$
2.97 – 3.29	( 1.910	0.007	0.069	0.016	0.001	0.071 ) $\times 10^{-1}$
3.29 – 3.64	( 1.691	0.006	0.060	0.012	0.000	0.062 ) $\times 10^{-1}$
3.64 – 4.02	( 1.461	0.005	0.052	0.010	0.001	0.052 ) $\times 10^{-1}$
4.02 – 4.43	( 1.248	0.004	0.044	0.007	0.001	0.044 ) $\times 10^{-1}$
4.43 – 4.88	( 1.079	0.004	0.037	0.006	0.001	0.038 ) $\times 10^{-1}$
4.88 – 5.37	( 9.127	0.029	0.315	0.042	0.015	0.318 ) $\times 10^{-2}$
5.37 – 5.90	( 7.700	0.024	0.265	0.032	0.014	0.267 ) $\times 10^{-2}$
5.90 – 6.47	( 6.485	0.020	0.223	0.024	0.013	0.224 ) $\times 10^{-2}$
6.47 – 7.09	( 5.388	0.017	0.185	0.018	0.012	0.186 ) $\times 10^{-2}$
7.09 – 7.76	( 4.431	0.014	0.152	0.013	0.011	0.153 ) $\times 10^{-2}$
7.76 – 8.48	( 3.683	0.011	0.126	0.010	0.009	0.127 ) $\times 10^{-2}$
8.48 – 9.26	( 3.054	0.010	0.105	0.008	0.008	0.105 ) $\times 10^{-2}$
9.26 – 10.1	( 2.483	0.008	0.085	0.006	0.007	0.085 ) $\times 10^{-2}$
10.1 – 11.0	( 2.034	0.007	0.070	0.005	0.006	0.070 ) $\times 10^{-2}$
11.0 – 12.0	( 1.665	0.006	0.057	0.004	0.005	0.057 ) $\times 10^{-2}$
12.0 – 13.0	( 1.354	0.005	0.046	0.003	0.004	0.047 ) $\times 10^{-2}$
13.0 – 14.1	( 1.116	0.004	0.038	0.002	0.004	0.038 ) $\times 10^{-2}$
14.1 – 15.3	( 9.138	0.038	0.313	0.020	0.030	0.315 ) $\times 10^{-3}$
15.3 – 16.6	( 7.424	0.032	0.254	0.016	0.025	0.256 ) $\times 10^{-3}$
16.6 – 18.0	( 6.105	0.027	0.209	0.014	0.021	0.211 ) $\times 10^{-3}$
18.0 – 19.5	( 4.991	0.023	0.171	0.012	0.017	0.172 ) $\times 10^{-3}$
19.5 – 21.1	( 4.048	0.019	0.139	0.010	0.014	0.140 ) $\times 10^{-3}$
21.1 – 22.8	( 3.323	0.016	0.114	0.009	0.012	0.115 ) $\times 10^{-3}$
22.8 – 24.7	( 2.741	0.013	0.094	0.008	0.010	0.095 ) $\times 10^{-3}$
24.7 – 26.7	( 2.224	0.011	0.076	0.007	0.008	0.077 ) $\times 10^{-3}$
26.7 – 28.8	( 1.829	0.010	0.063	0.006	0.007	0.063 ) $\times 10^{-3}$
28.8 – 33.5	( 1.344	0.005	0.046	0.005	0.005	0.047 ) $\times 10^{-3}$
33.5 – 38.9	( 9.122	0.040	0.314	0.035	0.036	0.318 ) $\times 10^{-4}$
38.9 – 45.1	( 6.206	0.030	0.214	0.026	0.025	0.217 ) $\times 10^{-4}$
45.1 – 52.2	( 4.156	0.023	0.143	0.019	0.018	0.146 ) $\times 10^{-4}$
52.2 – 60.3	( 2.841	0.018	0.098	0.014	0.012	0.100 ) $\times 10^{-4}$
60.3 – 69.7	( 1.897	0.014	0.066	0.010	0.009	0.067 ) $\times 10^{-4}$
69.7 – 80.5	( 1.286	0.010	0.044	0.007	0.006	0.045 ) $\times 10^{-4}$
80.5 – 93.0	( 8.704	0.080	0.301	0.050	0.045	0.309 ) $\times 10^{-5}$

*Table continued*



TABLE SIII – (Continued).

Rigidity [GV]	$\Phi_{\text{Ne}}$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$
93.0 – 108	( 5.684	0.059	0.197	0.033	0.031	0.202 ) $\times 10^{-5}$
108 – 125	( 3.820	0.045	0.133	0.022	0.022	0.136 ) $\times 10^{-5}$
125 – 147	( 2.545	0.032	0.088	0.015	0.016	0.091 ) $\times 10^{-5}$
147 – 175	( 1.549	0.022	0.054	0.009	0.011	0.056 ) $\times 10^{-5}$
175 – 211	( 9.602	0.154	0.335	0.058	0.073	0.348 ) $\times 10^{-6}$
211 – 259	( 5.737	0.103	0.201	0.037	0.050	0.210 ) $\times 10^{-6}$
259 – 330	( 3.092	0.062	0.109	0.023	0.032	0.116 ) $\times 10^{-6}$
330 – 441	( 1.506	0.034	0.053	0.014	0.019	0.058 ) $\times 10^{-6}$
441 – 660	( 6.026	0.153	0.216	0.081	0.108	0.255 ) $\times 10^{-7}$
660 – 1200	( 1.628	0.049	0.060	0.038	0.052	0.088 ) $\times 10^{-7}$
1200 – 3000	( 2.753	0.294	0.129	0.047	0.135	0.193 ) $\times 10^{-8}$

TABLE SIV: The Mg flux  $\Phi_{\text{Mg}}$  as a function of rigidity at the top of AMS in units of  $[\text{m}^2 \cdot \text{sr} \cdot \text{s} \cdot \text{GV}]^{-1}$  including errors due to statistics (stat.); contributions to the systematic error from the trigger, background, and acceptance (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic error.

Rigidity [GV]	$\Phi_{\text{Mg}}$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$
2.15 – 2.40	( 3.190	0.014	0.130	0.041	0.015	0.137 ) $\times 10^{-1}$
2.40 – 2.67	( 2.933	0.011	0.115	0.034	0.009	0.120 ) $\times 10^{-1}$
2.67 – 2.97	( 2.623	0.009	0.100	0.027	0.004	0.104 ) $\times 10^{-1}$
2.97 – 3.29	( 2.308	0.008	0.086	0.021	0.002	0.089 ) $\times 10^{-1}$
3.29 – 3.64	( 2.048	0.007	0.075	0.017	0.000	0.077 ) $\times 10^{-1}$
3.64 – 4.02	( 1.776	0.006	0.064	0.013	0.001	0.066 ) $\times 10^{-1}$
4.02 – 4.43	( 1.524	0.005	0.055	0.010	0.001	0.056 ) $\times 10^{-1}$
4.43 – 4.88	( 1.299	0.004	0.046	0.008	0.002	0.047 ) $\times 10^{-1}$
4.88 – 5.37	( 1.101	0.003	0.039	0.006	0.002	0.040 ) $\times 10^{-1}$
5.37 – 5.90	( 9.257	0.026	0.328	0.043	0.017	0.331 ) $\times 10^{-2}$
5.90 – 6.47	( 7.702	0.022	0.272	0.033	0.016	0.275 ) $\times 10^{-2}$
6.47 – 7.09	( 6.407	0.018	0.226	0.025	0.014	0.228 ) $\times 10^{-2}$
7.09 – 7.76	( 5.294	0.015	0.187	0.019	0.013	0.188 ) $\times 10^{-2}$
7.76 – 8.48	( 4.383	0.012	0.155	0.014	0.011	0.156 ) $\times 10^{-2}$
8.48 – 9.26	( 3.605	0.010	0.127	0.011	0.010	0.128 ) $\times 10^{-2}$
9.26 – 10.1	( 2.953	0.009	0.104	0.009	0.008	0.105 ) $\times 10^{-2}$
10.1 – 11.0	( 2.425	0.007	0.085	0.007	0.007	0.086 ) $\times 10^{-2}$
11.0 – 12.0	( 1.970	0.006	0.069	0.005	0.006	0.070 ) $\times 10^{-2}$
12.0 – 13.0	( 1.622	0.006	0.057	0.004	0.005	0.058 ) $\times 10^{-2}$
13.0 – 14.1	( 1.334	0.005	0.047	0.004	0.004	0.047 ) $\times 10^{-2}$
14.1 – 15.3	( 1.100	0.004	0.039	0.003	0.004	0.039 ) $\times 10^{-2}$
15.3 – 16.6	( 8.966	0.035	0.316	0.025	0.030	0.318 ) $\times 10^{-3}$
16.6 – 18.0	( 7.332	0.030	0.258	0.021	0.025	0.260 ) $\times 10^{-3}$
18.0 – 19.5	( 6.012	0.025	0.212	0.017	0.021	0.214 ) $\times 10^{-3}$
19.5 – 21.1	( 4.907	0.021	0.173	0.015	0.017	0.174 ) $\times 10^{-3}$
21.1 – 22.8	( 4.014	0.018	0.141	0.012	0.015	0.143 ) $\times 10^{-3}$
22.8 – 24.7	( 3.253	0.014	0.115	0.011	0.012	0.116 ) $\times 10^{-3}$
24.7 – 26.7	( 2.668	0.012	0.094	0.009	0.010	0.095 ) $\times 10^{-3}$
26.7 – 28.8	( 2.181	0.010	0.077	0.008	0.008	0.078 ) $\times 10^{-3}$
28.8 – 33.5	( 1.638	0.006	0.058	0.006	0.006	0.059 ) $\times 10^{-3}$
33.5 – 38.9	( 1.105	0.004	0.039	0.004	0.004	0.040 ) $\times 10^{-3}$
38.9 – 45.1	( 7.413	0.033	0.263	0.032	0.030	0.267 ) $\times 10^{-4}$
45.1 – 52.2	( 5.011	0.025	0.178	0.023	0.021	0.181 ) $\times 10^{-4}$
52.2 – 60.3	( 3.412	0.020	0.122	0.017	0.015	0.124 ) $\times 10^{-4}$
60.3 – 69.7	( 2.294	0.015	0.082	0.012	0.011	0.083 ) $\times 10^{-4}$
69.7 – 80.5	( 1.534	0.011	0.055	0.008	0.007	0.056 ) $\times 10^{-4}$
80.5 – 93.0	( 1.045	0.009	0.038	0.006	0.005	0.038 ) $\times 10^{-4}$

*Table continued*

TABLE SIV – (Continued).

Rigidity [GV]	$\Phi_{Mg}$	$\sigma_{stat.}$	$\sigma_{acc.}$	$\sigma_{unf.}$	$\sigma_{scale}$	$\sigma_{syst.}$
93.0 – 108	( 6.959	0.065	0.250	0.037	0.037	0.256 ) $\times 10^{-5}$
108 – 125	( 4.628	0.050	0.167	0.025	0.026	0.171 ) $\times 10^{-5}$
125 – 147	( 3.040	0.035	0.110	0.016	0.019	0.112 ) $\times 10^{-5}$
147 – 175	( 1.894	0.025	0.069	0.010	0.013	0.070 ) $\times 10^{-5}$
175 – 211	( 1.155	0.017	0.042	0.006	0.009	0.043 ) $\times 10^{-5}$
211 – 259	( 6.782	0.112	0.248	0.039	0.059	0.257 ) $\times 10^{-6}$
259 – 330	( 3.711	0.068	0.136	0.026	0.039	0.144 ) $\times 10^{-6}$
330 – 441	( 1.759	0.037	0.065	0.017	0.024	0.071 ) $\times 10^{-6}$
441 – 660	( 7.276	0.171	0.273	0.107	0.139	0.324 ) $\times 10^{-7}$
660 – 1200	( 1.888	0.053	0.073	0.050	0.064	0.110 ) $\times 10^{-7}$
1200 – 3000	( 2.845	0.302	0.135	0.055	0.170	0.224 ) $\times 10^{-8}$

TABLE SV: The Si flux  $\Phi_{\text{Si}}$  as a function of rigidity at the top of AMS in units of  $[\text{m}^2 \cdot \text{sr} \cdot \text{s} \cdot \text{GV}]^{-1}$  including errors due to statistics (stat.); contributions to the systematic error from the trigger, background, and acceptance (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic error.

Rigidity [GV]	$\Phi_{\text{Si}}$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$
2.15 – 2.40	( 2.271	0.012	0.097	0.107	0.011	0.145 ) $\times 10^{-1}$
2.40 – 2.67	( 2.109	0.010	0.087	0.048	0.006	0.099 ) $\times 10^{-1}$
2.67 – 2.97	( 1.925	0.008	0.077	0.025	0.003	0.081 ) $\times 10^{-1}$
2.97 – 3.29	( 1.720	0.007	0.067	0.019	0.001	0.069 ) $\times 10^{-1}$
3.29 – 3.64	( 1.524	0.006	0.058	0.014	0.000	0.060 ) $\times 10^{-1}$
3.64 – 4.02	( 1.327	0.005	0.050	0.011	0.001	0.051 ) $\times 10^{-1}$
4.02 – 4.43	( 1.139	0.004	0.043	0.008	0.001	0.043 ) $\times 10^{-1}$
4.43 – 4.88	( 9.800	0.034	0.365	0.063	0.013	0.371 ) $\times 10^{-2}$
4.88 – 5.37	( 8.258	0.027	0.306	0.048	0.013	0.310 ) $\times 10^{-2}$
5.37 – 5.90	( 6.937	0.023	0.257	0.036	0.013	0.259 ) $\times 10^{-2}$
5.90 – 6.47	( 5.840	0.019	0.216	0.028	0.012	0.218 ) $\times 10^{-2}$
6.47 – 7.09	( 4.869	0.016	0.180	0.021	0.011	0.181 ) $\times 10^{-2}$
7.09 – 7.76	( 4.082	0.013	0.151	0.017	0.010	0.152 ) $\times 10^{-2}$
7.76 – 8.48	( 3.341	0.011	0.123	0.013	0.009	0.124 ) $\times 10^{-2}$
8.48 – 9.26	( 2.788	0.009	0.103	0.010	0.007	0.104 ) $\times 10^{-2}$
9.26 – 10.1	( 2.299	0.008	0.085	0.008	0.006	0.085 ) $\times 10^{-2}$
10.1 – 11.0	( 1.894	0.007	0.070	0.007	0.006	0.070 ) $\times 10^{-2}$
11.0 – 12.0	( 1.550	0.006	0.057	0.005	0.005	0.058 ) $\times 10^{-2}$
12.0 – 13.0	( 1.280	0.005	0.047	0.004	0.004	0.048 ) $\times 10^{-2}$
13.0 – 14.1	( 1.063	0.004	0.039	0.003	0.003	0.039 ) $\times 10^{-2}$
14.1 – 15.3	( 8.671	0.037	0.320	0.027	0.028	0.322 ) $\times 10^{-3}$
15.3 – 16.6	( 7.162	0.031	0.264	0.022	0.024	0.266 ) $\times 10^{-3}$
16.6 – 18.0	( 5.845	0.027	0.216	0.018	0.020	0.217 ) $\times 10^{-3}$
18.0 – 19.5	( 4.801	0.023	0.177	0.015	0.017	0.179 ) $\times 10^{-3}$
19.5 – 21.1	( 3.956	0.019	0.146	0.012	0.014	0.147 ) $\times 10^{-3}$
21.1 – 22.8	( 3.242	0.016	0.120	0.010	0.012	0.121 ) $\times 10^{-3}$
22.8 – 24.7	( 2.664	0.013	0.098	0.008	0.010	0.099 ) $\times 10^{-3}$
24.7 – 26.7	( 2.185	0.011	0.081	0.007	0.008	0.081 ) $\times 10^{-3}$
26.7 – 28.8	( 1.817	0.010	0.067	0.006	0.007	0.068 ) $\times 10^{-3}$
28.8 – 33.5	( 1.360	0.005	0.050	0.004	0.005	0.051 ) $\times 10^{-3}$
33.5 – 38.9	( 9.294	0.040	0.345	0.032	0.037	0.348 ) $\times 10^{-4}$
38.9 – 45.1	( 6.275	0.031	0.233	0.022	0.025	0.236 ) $\times 10^{-4}$
45.1 – 52.2	( 4.339	0.024	0.162	0.016	0.018	0.163 ) $\times 10^{-4}$
52.2 – 60.3	( 2.924	0.018	0.109	0.011	0.013	0.111 ) $\times 10^{-4}$
60.3 – 69.7	( 2.005	0.014	0.075	0.008	0.009	0.076 ) $\times 10^{-4}$
69.7 – 80.5	( 1.363	0.011	0.051	0.006	0.006	0.052 ) $\times 10^{-4}$
80.5 – 93.0	( 9.277	0.084	0.350	0.040	0.046	0.355 ) $\times 10^{-5}$
93.0 – 108	( 6.164	0.062	0.233	0.027	0.032	0.237 ) $\times 10^{-5}$

*Table continued*

TABLE SV – (Continued).

Rigidity [GV]	$\Phi_{Si}$	$\sigma_{stat.}$	$\sigma_{acc.}$	$\sigma_{unf.}$	$\sigma_{scale}$	$\sigma_{syst.}$
108 – 125	( 4.092	0.048	0.155	0.019	0.023	0.158 ) $\times 10^{-5}$
125 – 147	( 2.657	0.034	0.101	0.013	0.016	0.103 ) $\times 10^{-5}$
147 – 175	( 1.721	0.024	0.066	0.009	0.011	0.067 ) $\times 10^{-5}$
175 – 211	( 1.043	0.016	0.040	0.006	0.008	0.041 ) $\times 10^{-5}$
211 – 259	( 6.186	0.110	0.238	0.039	0.053	0.247 ) $\times 10^{-6}$
259 – 330	( 3.275	0.065	0.127	0.025	0.034	0.134 ) $\times 10^{-6}$
330 – 441	( 1.619	0.037	0.064	0.016	0.022	0.069 ) $\times 10^{-6}$
441 – 660	( 6.515	0.164	0.260	0.097	0.125	0.304 ) $\times 10^{-7}$
660 – 1200	( 1.754	0.052	0.073	0.047	0.060	0.105 ) $\times 10^{-7}$
1200 – 3000	( 2.369	0.282	0.124	0.043	0.136	0.189 ) $\times 10^{-8}$

TABLE SVI: The F flux  $\Phi_F$  as a function of rigidity at the top of AMS in units of  $[\text{m}^2 \cdot \text{sr} \cdot \text{s} \cdot \text{GV}]^{-1}$  including errors due to statistics (stat.); contributions to the systematic error from the trigger, background, and acceptance (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic error.

Rigidity [GV]	$\Phi_F$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$	
2.15 – 2.40	( 3.035	0.041	0.111	0.053	0.015	0.124 )	$\times 10^{-2}$
2.40 – 2.67	( 2.825	0.034	0.100	0.037	0.009	0.107 )	$\times 10^{-2}$
2.67 – 2.97	( 2.642	0.029	0.091	0.028	0.004	0.095 )	$\times 10^{-2}$
2.97 – 3.29	( 2.417	0.025	0.082	0.022	0.002	0.084 )	$\times 10^{-2}$
3.29 – 3.64	( 2.163	0.021	0.072	0.016	0.000	0.074 )	$\times 10^{-2}$
3.64 – 4.02	( 1.871	0.018	0.062	0.012	0.001	0.063 )	$\times 10^{-2}$
4.02 – 4.43	( 1.569	0.015	0.051	0.008	0.001	0.052 )	$\times 10^{-2}$
4.43 – 4.88	( 1.327	0.012	0.043	0.006	0.002	0.044 )	$\times 10^{-2}$
4.88 – 5.37	( 1.099	0.010	0.036	0.004	0.002	0.036 )	$\times 10^{-2}$
5.37 – 5.90	( 9.057	0.079	0.294	0.032	0.017	0.296 )	$\times 10^{-3}$
5.90 – 6.47	( 7.461	0.066	0.242	0.024	0.015	0.244 )	$\times 10^{-3}$
6.47 – 7.09	( 6.131	0.054	0.199	0.018	0.014	0.200 )	$\times 10^{-3}$
7.09 – 7.76	( 4.953	0.044	0.161	0.014	0.012	0.162 )	$\times 10^{-3}$
7.76 – 8.48	( 4.002	0.036	0.130	0.011	0.010	0.131 )	$\times 10^{-3}$
8.48 – 9.26	( 3.234	0.030	0.105	0.009	0.009	0.106 )	$\times 10^{-3}$
9.26 – 10.1	( 2.633	0.025	0.086	0.007	0.007	0.086 )	$\times 10^{-3}$
10.1 – 11.0	( 2.136	0.022	0.069	0.006	0.006	0.070 )	$\times 10^{-3}$
11.0 – 12.0	( 1.680	0.018	0.055	0.005	0.005	0.055 )	$\times 10^{-3}$
12.0 – 13.0	( 1.363	0.016	0.044	0.004	0.004	0.045 )	$\times 10^{-3}$
13.0 – 14.1	( 1.101	0.013	0.036	0.003	0.004	0.036 )	$\times 10^{-3}$
14.1 – 15.3	( 8.966	0.114	0.292	0.027	0.029	0.295 )	$\times 10^{-4}$
15.3 – 16.6	( 7.182	0.096	0.234	0.022	0.024	0.237 )	$\times 10^{-4}$
16.6 – 18.0	( 5.730	0.081	0.187	0.018	0.020	0.189 )	$\times 10^{-4}$
18.0 – 19.5	( 4.552	0.068	0.149	0.015	0.016	0.151 )	$\times 10^{-4}$
19.5 – 21.1	( 3.707	0.057	0.121	0.013	0.013	0.123 )	$\times 10^{-4}$
21.1 – 22.8	( 2.944	0.047	0.097	0.010	0.011	0.098 )	$\times 10^{-4}$
22.8 – 24.7	( 2.465	0.039	0.081	0.009	0.009	0.082 )	$\times 10^{-4}$
24.7 – 26.7	( 1.896	0.032	0.063	0.007	0.007	0.063 )	$\times 10^{-4}$
26.7 – 28.8	( 1.536	0.027	0.051	0.006	0.006	0.052 )	$\times 10^{-4}$
28.8 – 33.5	( 1.085	0.015	0.036	0.004	0.004	0.037 )	$\times 10^{-4}$
33.5 – 38.9	( 7.080	0.107	0.239	0.031	0.029	0.242 )	$\times 10^{-5}$
38.9 – 45.1	( 4.648	0.081	0.158	0.022	0.020	0.161 )	$\times 10^{-5}$
45.1 – 52.2	( 3.002	0.060	0.103	0.015	0.014	0.105 )	$\times 10^{-5}$
52.2 – 60.3	( 1.918	0.045	0.067	0.010	0.009	0.068 )	$\times 10^{-5}$
60.3 – 69.7	( 1.205	0.033	0.042	0.007	0.006	0.043 )	$\times 10^{-5}$
69.7 – 80.5	( 7.890	0.248	0.279	0.048	0.042	0.286 )	$\times 10^{-6}$
80.5 – 93.0	( 5.164	0.187	0.184	0.033	0.030	0.190 )	$\times 10^{-6}$
93.0 – 108	( 3.020	0.129	0.109	0.020	0.019	0.112 )	$\times 10^{-6}$

*Table continued*

TABLE SVI – (Continued).

Rigidity [GV]	$\Phi_F$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{sys.}}$	
108 – 125	( 2.202	0.104	0.080	0.015	0.015	0.083 )	$\times 10^{-6}$
125 – 147	( 1.429	0.073	0.053	0.011	0.011	0.055 )	$\times 10^{-6}$
147 – 175	( 7.812	0.476	0.291	0.064	0.066	0.305 )	$\times 10^{-7}$
175 – 211	( 4.342	0.314	0.164	0.042	0.042	0.174 )	$\times 10^{-7}$
211 – 259	( 2.775	0.216	0.106	0.033	0.032	0.116 )	$\times 10^{-7}$
259 – 330	( 1.458	0.126	0.057	0.024	0.021	0.065 )	$\times 10^{-7}$
330 – 441	( 6.036	0.661	0.242	0.145	0.110	0.303 )	$\times 10^{-8}$
441 – 660	( 2.316	0.285	0.097	0.091	0.059	0.146 )	$\times 10^{-8}$
660 – 1200	( 5.637	0.862	0.264	0.436	0.240	0.563 )	$\times 10^{-9}$
1200 – 3000	( 5.279	3.931	0.410	0.366	0.392	0.675 )	$\times 10^{-10}$

TABLE SVII: The C flux  $\Phi_C$  as a function of rigidity at the top of AMS in units of  $[\text{m}^2 \cdot \text{sr} \cdot \text{s} \cdot \text{GV}]^{-1}$  including errors due to statistics (stat.); contributions to the systematic error from the trigger, background, and acceptance (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic error.

Rigidity [GV]	$\Phi_C$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$	
2.15 – 2.40	( 1.793	0.003	0.047	0.020	0.006	0.052 )	$\times 10^0$
2.40 – 2.67	( 1.677	0.002	0.043	0.015	0.003	0.045 )	$\times 10^0$
2.67 – 2.97	( 1.504	0.002	0.037	0.011	0.001	0.039 )	$\times 10^0$
2.97 – 3.29	( 1.313	0.002	0.032	0.008	0.000	0.033 )	$\times 10^0$
3.29 – 3.64	( 1.132	0.001	0.027	0.006	0.000	0.028 )	$\times 10^0$
3.64 – 4.02	( 9.665	0.012	0.228	0.044	0.007	0.232 )	$\times 10^{-1}$
4.02 – 4.43	( 8.209	0.010	0.192	0.032	0.009	0.195 )	$\times 10^{-1}$
4.43 – 4.88	( 6.929	0.008	0.160	0.023	0.009	0.162 )	$\times 10^{-1}$
4.88 – 5.37	( 5.796	0.007	0.133	0.017	0.010	0.135 )	$\times 10^{-1}$
5.37 – 5.90	( 4.820	0.005	0.110	0.012	0.009	0.111 )	$\times 10^{-1}$
5.90 – 6.47	( 4.013	0.005	0.091	0.009	0.009	0.092 )	$\times 10^{-1}$
6.47 – 7.09	( 3.300	0.004	0.075	0.007	0.008	0.076 )	$\times 10^{-1}$
7.09 – 7.76	( 2.707	0.003	0.061	0.005	0.007	0.062 )	$\times 10^{-1}$
7.76 – 8.48	( 2.217	0.003	0.050	0.004	0.006	0.051 )	$\times 10^{-1}$
8.48 – 9.26	( 1.811	0.002	0.041	0.003	0.005	0.041 )	$\times 10^{-1}$
9.26 – 10.1	( 1.475	0.002	0.033	0.003	0.005	0.034 )	$\times 10^{-1}$
10.1 – 11.0	( 1.203	0.002	0.027	0.002	0.004	0.028 )	$\times 10^{-1}$
11.0 – 12.0	( 9.762	0.013	0.220	0.018	0.033	0.224 )	$\times 10^{-2}$
12.0 – 13.0	( 7.961	0.011	0.180	0.015	0.027	0.182 )	$\times 10^{-2}$
13.0 – 14.1	( 6.543	0.010	0.148	0.013	0.023	0.150 )	$\times 10^{-2}$
14.1 – 15.3	( 5.348	0.008	0.121	0.011	0.019	0.123 )	$\times 10^{-2}$
15.3 – 16.6	( 4.362	0.007	0.099	0.009	0.016	0.100 )	$\times 10^{-2}$
16.6 – 18.0	( 3.558	0.006	0.081	0.008	0.013	0.082 )	$\times 10^{-2}$
18.0 – 19.5	( 2.904	0.005	0.066	0.007	0.011	0.067 )	$\times 10^{-2}$
19.5 – 21.1	( 2.375	0.004	0.054	0.006	0.009	0.055 )	$\times 10^{-2}$
21.1 – 22.8	( 1.939	0.004	0.044	0.005	0.007	0.045 )	$\times 10^{-2}$
22.8 – 24.7	( 1.585	0.003	0.036	0.005	0.006	0.037 )	$\times 10^{-2}$
24.7 – 26.7	( 1.286	0.002	0.029	0.004	0.005	0.030 )	$\times 10^{-2}$
26.7 – 28.8	( 1.052	0.002	0.024	0.003	0.004	0.025 )	$\times 10^{-2}$
28.8 – 31.1	( 8.599	0.017	0.197	0.030	0.034	0.202 )	$\times 10^{-3}$
31.1 – 33.5	( 7.045	0.015	0.162	0.026	0.028	0.166 )	$\times 10^{-3}$
33.5 – 36.1	( 5.789	0.013	0.133	0.022	0.024	0.137 )	$\times 10^{-3}$
36.1 – 38.9	( 4.743	0.011	0.109	0.019	0.020	0.113 )	$\times 10^{-3}$
38.9 – 41.9	( 3.896	0.010	0.090	0.016	0.016	0.093 )	$\times 10^{-3}$
41.9 – 45.1	( 3.175	0.009	0.073	0.014	0.014	0.076 )	$\times 10^{-3}$
45.1 – 48.5	( 2.618	0.008	0.061	0.012	0.011	0.063 )	$\times 10^{-3}$
48.5 – 52.2	( 2.160	0.007	0.050	0.010	0.009	0.052 )	$\times 10^{-3}$
52.2 – 56.1	( 1.779	0.006	0.041	0.009	0.008	0.043 )	$\times 10^{-3}$

*Table continued*



TABLE SVII – (Continued).

Rigidity [GV]	$\Phi_C$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$
56.1 – 60.3	( 1.460	0.005	0.034	0.007	0.007	0.035 ) $\times 10^{-3}$
60.3 – 64.8	( 1.189	0.004	0.028	0.006	0.005	0.029 ) $\times 10^{-3}$
64.8 – 69.7	( 9.794	0.039	0.229	0.053	0.046	0.240 ) $\times 10^{-4}$
69.7 – 74.9	( 8.018	0.034	0.188	0.044	0.038	0.197 ) $\times 10^{-4}$
74.9 – 80.5	( 6.641	0.030	0.156	0.037	0.032	0.164 ) $\times 10^{-4}$
80.5 – 86.5	( 5.369	0.026	0.126	0.031	0.027	0.133 ) $\times 10^{-4}$
86.5 – 93.0	( 4.448	0.023	0.105	0.026	0.023	0.110 ) $\times 10^{-4}$
93.0 – 100	( 3.593	0.020	0.085	0.022	0.019	0.090 ) $\times 10^{-4}$
100 – 108	( 2.965	0.017	0.070	0.018	0.016	0.074 ) $\times 10^{-4}$
108 – 116	( 2.419	0.015	0.057	0.015	0.013	0.061 ) $\times 10^{-4}$
116 – 125	( 1.975	0.013	0.047	0.012	0.011	0.050 ) $\times 10^{-4}$
125 – 135	( 1.596	0.011	0.038	0.010	0.009	0.040 ) $\times 10^{-4}$
135 – 147	( 1.289	0.009	0.031	0.008	0.008	0.033 ) $\times 10^{-4}$
147 – 160	( 9.980	0.075	0.238	0.066	0.061	0.254 ) $\times 10^{-5}$
160 – 175	( 7.906	0.062	0.189	0.053	0.050	0.203 ) $\times 10^{-5}$
175 – 192	( 6.154	0.051	0.147	0.043	0.041	0.159 ) $\times 10^{-5}$
192 – 211	( 4.839	0.043	0.116	0.035	0.034	0.126 ) $\times 10^{-5}$
211 – 233	( 3.712	0.035	0.089	0.029	0.028	0.098 ) $\times 10^{-5}$
233 – 259	( 2.854	0.028	0.069	0.024	0.023	0.076 ) $\times 10^{-5}$
259 – 291	( 2.118	0.022	0.051	0.019	0.019	0.058 ) $\times 10^{-5}$
291 – 330	( 1.521	0.017	0.037	0.015	0.015	0.043 ) $\times 10^{-5}$
330 – 379	( 1.079	0.013	0.026	0.012	0.013	0.032 ) $\times 10^{-5}$
379 – 441	( 7.186	0.091	0.177	0.095	0.099	0.224 ) $\times 10^{-6}$
441 – 525	( 4.871	0.065	0.121	0.077	0.083	0.166 ) $\times 10^{-6}$
525 – 660	( 2.853	0.039	0.072	0.056	0.064	0.111 ) $\times 10^{-6}$
660 – 880	( 1.446	0.022	0.037	0.037	0.045	0.069 ) $\times 10^{-6}$
880 – 1300	( 5.852	0.100	0.157	0.206	0.264	0.370 ) $\times 10^{-7}$
1300 – 3300	( 1.170	0.047	0.041	0.041	0.066	0.088 ) $\times 10^{-7}$

TABLE SVIII: The O flux  $\Phi_{\text{O}}$  as a function of rigidity at the top of AMS in units of  $[\text{m}^2 \cdot \text{sr} \cdot \text{s} \cdot \text{GV}]^{-1}$  including errors due to statistics (stat.); contributions to the systematic error from the trigger, background, and acceptance (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic error.

Rigidity [GV]	$\Phi_{\text{O}}$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$	
2.15 – 2.40	( 1.658	0.003	0.052	0.020	0.008	0.057 )	$\times 10^0$
2.40 – 2.67	( 1.524	0.002	0.046	0.015	0.005	0.049 )	$\times 10^0$
2.67 – 2.97	( 1.375	0.002	0.040	0.012	0.002	0.042 )	$\times 10^0$
2.97 – 3.29	( 1.215	0.002	0.034	0.009	0.001	0.035 )	$\times 10^0$
3.29 – 3.64	( 1.057	0.001	0.029	0.007	0.000	0.030 )	$\times 10^0$
3.64 – 4.02	( 9.097	0.012	0.248	0.048	0.005	0.253 )	$\times 10^{-1}$
4.02 – 4.43	( 7.730	0.010	0.209	0.035	0.007	0.212 )	$\times 10^{-1}$
4.43 – 4.88	( 6.546	0.008	0.176	0.025	0.008	0.178 )	$\times 10^{-1}$
4.88 – 5.37	( 5.493	0.007	0.147	0.018	0.009	0.148 )	$\times 10^{-1}$
5.37 – 5.90	( 4.578	0.006	0.122	0.013	0.009	0.123 )	$\times 10^{-1}$
5.90 – 6.47	( 3.809	0.005	0.101	0.010	0.008	0.102 )	$\times 10^{-1}$
6.47 – 7.09	( 3.153	0.004	0.084	0.007	0.007	0.085 )	$\times 10^{-1}$
7.09 – 7.76	( 2.591	0.003	0.069	0.006	0.006	0.070 )	$\times 10^{-1}$
7.76 – 8.48	( 2.134	0.003	0.057	0.004	0.005	0.057 )	$\times 10^{-1}$
8.48 – 9.26	( 1.752	0.002	0.047	0.003	0.005	0.047 )	$\times 10^{-1}$
9.26 – 10.1	( 1.434	0.002	0.038	0.003	0.004	0.039 )	$\times 10^{-1}$
10.1 – 11.0	( 1.173	0.002	0.031	0.002	0.003	0.032 )	$\times 10^{-1}$
11.0 – 12.0	( 9.600	0.013	0.257	0.018	0.029	0.260 )	$\times 10^{-2}$
12.0 – 13.0	( 7.874	0.012	0.211	0.015	0.024	0.213 )	$\times 10^{-2}$
13.0 – 14.1	( 6.465	0.010	0.174	0.013	0.021	0.175 )	$\times 10^{-2}$
14.1 – 15.3	( 5.302	0.009	0.143	0.011	0.017	0.144 )	$\times 10^{-2}$
15.3 – 16.6	( 4.356	0.007	0.117	0.009	0.015	0.119 )	$\times 10^{-2}$
16.6 – 18.0	( 3.562	0.006	0.096	0.008	0.012	0.097 )	$\times 10^{-2}$
18.0 – 19.5	( 2.929	0.005	0.079	0.007	0.010	0.080 )	$\times 10^{-2}$
19.5 – 21.1	( 2.403	0.004	0.065	0.006	0.009	0.066 )	$\times 10^{-2}$
21.1 – 22.8	( 1.975	0.004	0.054	0.005	0.007	0.054 )	$\times 10^{-2}$
22.8 – 24.7	( 1.611	0.003	0.044	0.004	0.006	0.044 )	$\times 10^{-2}$
24.7 – 26.7	( 1.316	0.003	0.036	0.004	0.005	0.036 )	$\times 10^{-2}$
26.7 – 28.8	( 1.078	0.002	0.029	0.003	0.004	0.030 )	$\times 10^{-2}$
28.8 – 31.1	( 8.906	0.019	0.243	0.028	0.034	0.247 )	$\times 10^{-3}$
31.1 – 33.5	( 7.341	0.016	0.201	0.024	0.029	0.204 )	$\times 10^{-3}$
33.5 – 36.1	( 6.022	0.014	0.165	0.021	0.024	0.168 )	$\times 10^{-3}$
36.1 – 38.9	( 4.972	0.012	0.137	0.018	0.020	0.139 )	$\times 10^{-3}$
38.9 – 41.9	( 4.056	0.011	0.112	0.015	0.016	0.114 )	$\times 10^{-3}$
41.9 – 45.1	( 3.351	0.009	0.093	0.013	0.014	0.095 )	$\times 10^{-3}$
45.1 – 48.5	( 2.773	0.008	0.077	0.011	0.012	0.079 )	$\times 10^{-3}$
48.5 – 52.2	( 2.283	0.007	0.064	0.010	0.010	0.065 )	$\times 10^{-3}$

*Table continued*

TABLE SVIII – (Continued).

Rigidity [GV]	$\Phi_{\text{O}}$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$
52.2 – 56.1	( 1.887	0.006	0.053	0.008	0.008	0.054 ) $\times 10^{-3}$
56.1 – 60.3	( 1.550	0.006	0.044	0.007	0.007	0.045 ) $\times 10^{-3}$
60.3 – 64.8	( 1.277	0.005	0.036	0.006	0.006	0.037 ) $\times 10^{-3}$
64.8 – 69.7	( 1.050	0.004	0.030	0.005	0.005	0.031 ) $\times 10^{-3}$
69.7 – 74.9	( 8.595	0.037	0.245	0.042	0.040	0.252 ) $\times 10^{-4}$
74.9 – 80.5	( 7.061	0.032	0.202	0.035	0.034	0.208 ) $\times 10^{-4}$
80.5 – 86.5	( 5.848	0.028	0.168	0.030	0.029	0.173 ) $\times 10^{-4}$
86.5 – 93.0	( 4.791	0.025	0.139	0.025	0.024	0.143 ) $\times 10^{-4}$
93.0 – 100	( 3.939	0.021	0.115	0.021	0.020	0.118 ) $\times 10^{-4}$
100 – 108	( 3.221	0.018	0.094	0.018	0.017	0.097 ) $\times 10^{-4}$
108 – 116	( 2.631	0.016	0.077	0.015	0.014	0.080 ) $\times 10^{-4}$
116 – 125	( 2.176	0.014	0.064	0.012	0.012	0.067 ) $\times 10^{-4}$
125 – 135	( 1.757	0.012	0.052	0.010	0.010	0.054 ) $\times 10^{-4}$
135 – 147	( 1.416	0.010	0.043	0.008	0.009	0.044 ) $\times 10^{-4}$
147 – 160	( 1.117	0.008	0.034	0.007	0.007	0.035 ) $\times 10^{-4}$
160 – 175	( 8.759	0.069	0.267	0.054	0.058	0.279 ) $\times 10^{-5}$
175 – 192	( 6.959	0.058	0.214	0.045	0.049	0.224 ) $\times 10^{-5}$
192 – 211	( 5.418	0.048	0.168	0.037	0.041	0.177 ) $\times 10^{-5}$
211 – 233	( 4.161	0.039	0.131	0.030	0.034	0.138 ) $\times 10^{-5}$
233 – 259	( 3.171	0.031	0.101	0.025	0.028	0.107 ) $\times 10^{-5}$
259 – 291	( 2.370	0.025	0.076	0.020	0.023	0.082 ) $\times 10^{-5}$
291 – 330	( 1.688	0.019	0.055	0.016	0.019	0.060 ) $\times 10^{-5}$
330 – 379	( 1.197	0.014	0.040	0.013	0.015	0.044 ) $\times 10^{-5}$
379 – 441	( 8.146	0.103	0.275	0.108	0.120	0.319 ) $\times 10^{-6}$
441 – 525	( 5.194	0.071	0.179	0.084	0.093	0.219 ) $\times 10^{-6}$
525 – 660	( 3.069	0.043	0.109	0.063	0.070	0.144 ) $\times 10^{-6}$
660 – 880	( 1.579	0.024	0.058	0.044	0.048	0.087 ) $\times 10^{-6}$
880 – 1300	( 6.737	0.115	0.261	0.273	0.282	0.472 ) $\times 10^{-7}$
1300 – 3300	( 1.191	0.052	0.057	0.045	0.061	0.095 ) $\times 10^{-7}$

TABLE SIX: The B flux  $\Phi_B$  as a function of rigidity at the top of AMS in units of  $[\text{m}^2 \cdot \text{sr} \cdot \text{s} \cdot \text{GV}]^{-1}$  including errors due to statistics (stat.); contributions to the systematic error from the trigger, background, and acceptance (acc.); the rigidity resolution function and unfolding (unf.); the absolute rigidity scale (scale); and the total systematic error (syst.). The contribution of individual sources to the systematic error are added in quadrature to arrive at the total systematic error.

Rigidity [GV]	$\Phi_B$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$
2.15 – 2.40	( 5.117	0.015	0.254	0.049	0.018	0.259 ) $\times 10^{-1}$
2.40 – 2.67	( 4.927	0.013	0.221	0.039	0.011	0.224 ) $\times 10^{-1}$
2.67 – 2.97	( 4.549	0.011	0.185	0.030	0.006	0.188 ) $\times 10^{-1}$
2.97 – 3.29	( 4.058	0.010	0.151	0.023	0.002	0.153 ) $\times 10^{-1}$
3.29 – 3.64	( 3.575	0.008	0.123	0.017	0.001	0.124 ) $\times 10^{-1}$
3.64 – 4.02	( 3.094	0.007	0.099	0.013	0.002	0.100 ) $\times 10^{-1}$
4.02 – 4.43	( 2.629	0.006	0.080	0.010	0.003	0.080 ) $\times 10^{-1}$
4.43 – 4.88	( 2.202	0.005	0.063	0.008	0.004	0.064 ) $\times 10^{-1}$
4.88 – 5.37	( 1.831	0.004	0.050	0.006	0.004	0.051 ) $\times 10^{-1}$
5.37 – 5.90	( 1.506	0.003	0.040	0.005	0.004	0.040 ) $\times 10^{-1}$
5.90 – 6.47	( 1.229	0.002	0.032	0.004	0.003	0.032 ) $\times 10^{-1}$
6.47 – 7.09	( 1.000	0.002	0.025	0.003	0.003	0.026 ) $\times 10^{-1}$
7.09 – 7.76	( 8.024	0.017	0.199	0.024	0.025	0.201 ) $\times 10^{-2}$
7.76 – 8.48	( 6.478	0.014	0.158	0.019	0.021	0.160 ) $\times 10^{-2}$
8.48 – 9.26	( 5.228	0.011	0.126	0.016	0.018	0.128 ) $\times 10^{-2}$
9.26 – 10.1	( 4.182	0.009	0.100	0.013	0.015	0.102 ) $\times 10^{-2}$
10.1 – 11.0	( 3.351	0.008	0.080	0.010	0.012	0.081 ) $\times 10^{-2}$
11.0 – 12.0	( 2.671	0.007	0.063	0.008	0.010	0.064 ) $\times 10^{-2}$
12.0 – 13.0	( 2.135	0.006	0.050	0.006	0.008	0.051 ) $\times 10^{-2}$
13.0 – 14.1	( 1.714	0.005	0.040	0.005	0.007	0.041 ) $\times 10^{-2}$
14.1 – 15.3	( 1.374	0.004	0.032	0.004	0.006	0.033 ) $\times 10^{-2}$
15.3 – 16.6	( 1.095	0.003	0.026	0.003	0.005	0.026 ) $\times 10^{-2}$
16.6 – 18.0	( 8.680	0.029	0.204	0.024	0.038	0.209 ) $\times 10^{-3}$
18.0 – 19.5	( 6.960	0.024	0.164	0.019	0.031	0.168 ) $\times 10^{-3}$
19.5 – 21.1	( 5.548	0.020	0.131	0.015	0.025	0.134 ) $\times 10^{-3}$
21.1 – 22.8	( 4.419	0.017	0.105	0.012	0.020	0.107 ) $\times 10^{-3}$
22.8 – 24.7	( 3.508	0.014	0.083	0.009	0.017	0.085 ) $\times 10^{-3}$
24.7 – 26.7	( 2.800	0.011	0.067	0.007	0.013	0.068 ) $\times 10^{-3}$
26.7 – 28.8	( 2.233	0.009	0.054	0.006	0.011	0.055 ) $\times 10^{-3}$
28.8 – 31.1	( 1.770	0.008	0.043	0.004	0.009	0.044 ) $\times 10^{-3}$
31.1 – 33.5	( 1.410	0.007	0.034	0.004	0.007	0.035 ) $\times 10^{-3}$
33.5 – 36.1	( 1.137	0.006	0.028	0.003	0.006	0.028 ) $\times 10^{-3}$
36.1 – 38.9	( 9.006	0.049	0.221	0.023	0.047	0.227 ) $\times 10^{-4}$
38.9 – 41.9	( 7.117	0.042	0.176	0.019	0.038	0.181 ) $\times 10^{-4}$
41.9 – 45.1	( 5.721	0.036	0.142	0.016	0.031	0.147 ) $\times 10^{-4}$
45.1 – 48.5	( 4.616	0.032	0.116	0.013	0.025	0.119 ) $\times 10^{-4}$
48.5 – 52.2	( 3.666	0.027	0.093	0.011	0.021	0.096 ) $\times 10^{-4}$
52.2 – 56.1	( 2.955	0.024	0.075	0.009	0.017	0.078 ) $\times 10^{-4}$

*Table continued*

TABLE SIX – (Continued).

Rigidity [GV]	$\Phi_B$	$\sigma_{\text{stat.}}$	$\sigma_{\text{acc.}}$	$\sigma_{\text{unf.}}$	$\sigma_{\text{scale}}$	$\sigma_{\text{syst.}}$
56.1 – 60.3	( 2.362	0.020	0.061	0.008	0.014	0.063 ) $\times 10^{-4}$
60.3 – 64.8	( 1.885	0.018	0.049	0.007	0.011	0.051 ) $\times 10^{-4}$
64.8 – 69.7	( 1.508	0.015	0.040	0.006	0.009	0.041 ) $\times 10^{-4}$
69.7 – 74.9	( 1.204	0.013	0.032	0.005	0.008	0.033 ) $\times 10^{-4}$
74.9 – 80.5	( 9.570	0.112	0.256	0.043	0.061	0.266 ) $\times 10^{-5}$
80.5 – 86.5	( 7.660	0.096	0.207	0.037	0.050	0.216 ) $\times 10^{-5}$
86.5 – 93.0	( 6.225	0.083	0.170	0.033	0.042	0.178 ) $\times 10^{-5}$
93.0 – 100	( 4.880	0.071	0.135	0.028	0.034	0.142 ) $\times 10^{-5}$
100 – 108	( 3.762	0.058	0.105	0.023	0.027	0.111 ) $\times 10^{-5}$
108 – 116	( 3.081	0.053	0.087	0.021	0.023	0.092 ) $\times 10^{-5}$
116 – 125	( 2.450	0.044	0.070	0.018	0.019	0.075 ) $\times 10^{-5}$
125 – 135	( 1.915	0.037	0.055	0.016	0.015	0.060 ) $\times 10^{-5}$
135 – 147	( 1.510	0.030	0.044	0.014	0.013	0.048 ) $\times 10^{-5}$
147 – 160	( 1.148	0.025	0.034	0.011	0.010	0.037 ) $\times 10^{-5}$
160 – 175	( 8.909	0.206	0.268	0.098	0.084	0.298 ) $\times 10^{-6}$
175 – 192	( 6.769	0.168	0.206	0.083	0.068	0.233 ) $\times 10^{-6}$
192 – 211	( 5.105	0.138	0.158	0.070	0.056	0.181 ) $\times 10^{-6}$
211 – 233	( 3.868	0.112	0.121	0.059	0.046	0.142 ) $\times 10^{-6}$
233 – 259	( 2.812	0.087	0.089	0.048	0.036	0.108 ) $\times 10^{-6}$
259 – 291	( 2.036	0.067	0.065	0.040	0.029	0.082 ) $\times 10^{-6}$
291 – 330	( 1.360	0.050	0.044	0.030	0.022	0.058 ) $\times 10^{-6}$
330 – 379	( 9.254	0.364	0.300	0.238	0.171	0.419 ) $\times 10^{-7}$
379 – 441	( 6.402	0.269	0.208	0.192	0.137	0.315 ) $\times 10^{-7}$
441 – 525	( 3.933	0.181	0.128	0.141	0.099	0.214 ) $\times 10^{-7}$
525 – 660	( 2.143	0.105	0.070	0.095	0.066	0.135 ) $\times 10^{-7}$
660 – 880	( 1.106	0.059	0.036	0.065	0.044	0.087 ) $\times 10^{-7}$
880 – 1300	( 4.625	0.278	0.153	0.388	0.249	0.486 ) $\times 10^{-8}$
1300 – 3300	( 6.177	1.037	0.290	0.506	0.412	0.714 ) $\times 10^{-9}$

TABLE SX. The Ne/Si, Na/Si, Mg/Si, Al/Si, S/Si, C/O, and N/O abundance ratios at the source. The AMS data are from Table I. For Ref. [6] ratio values and errors were calculated from Table 6. For errors "Combined Errors" column was used. Errors were propagated in quadrature. For Ref. [37] ratio values and errors were calculated from Table 1 "This work, Calculated GCR Source" column. Errors were propagated in quadrature. For Ref. [38] ratio values and errors were calculated from Table 5. For values "Mean" column was used. For errors "Variance" column was used. Errors were propagated in quadrature. For Ref. [39] ratio values and errors were calculated from Table 2. For errors "Total Statistical & Systematic" column was used. Errors were propagated in quadrature.

Abundance Ratio	AMS	Ref. [6]	Ref. [37]	Ref. [38]	Ref. [39]
$\Phi_{\text{Ne}}/\Phi_{\text{Si}}$	$0.833 \pm 0.025$	$0.580 \pm 0.030$	$0.580 \pm 0.061$	$0.581 \pm 0.004$	$0.511 \pm 0.058$
$\Phi_{\text{Na}}/\Phi_{\text{Si}}$	$0.036 \pm 0.003$	$0.0323 \pm 0.0097$	$0.0324^{+0.0130}_{-0.0077}$	$0.040 \pm 0.003$	$0.0372 \pm 0.0256$
$\Phi_{\text{Mg}}/\Phi_{\text{Si}}$	$0.994 \pm 0.029$	$1.038 \pm 0.028$	$1.080 \pm 0.040$	$1.110 \pm 0.011$	$1.111 \pm 0.033$
$\Phi_{\text{Al}}/\Phi_{\text{Si}}$	$0.103 \pm 0.004$	$0.0778 \pm 0.012$	$0.0778^{+0.0130}_{-0.0100}$	$0.0966 \pm 0.0083$	$0.104 \pm 0.019$
$\Phi_{\text{S}}/\Phi_{\text{Si}}$	$0.167 \pm 0.006$	$0.131 \pm 0.009$	$0.131 \pm 0.002$	$0.131 \pm 0.002$	$0.129 \pm 0.019$
$\Phi_{\text{C}}/\Phi_{\text{O}}$	$0.836 \pm 0.025$	$0.807 \pm 0.015$	$0.850^{+0.066}_{-0.064}$	$0.800 \pm 0.029$	$0.760 \pm 0.029$
$\Phi_{\text{N}}/\Phi_{\text{O}}$	$0.092 \pm 0.002$	$0.048 \pm 0.012$	$0.065 \pm 0.006$	$0.072 \pm 0.004$	$0.053 \pm 0.037$

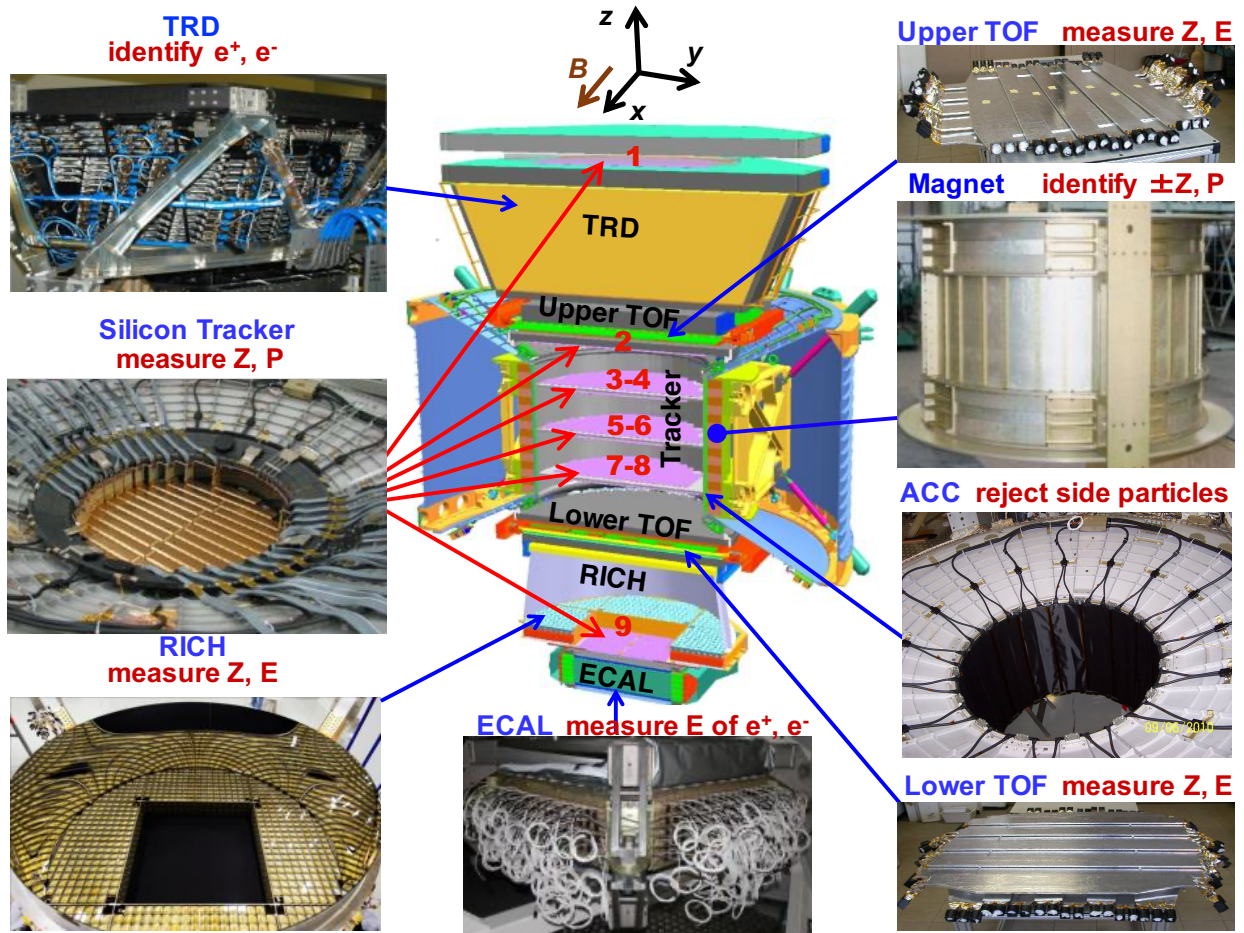


FIG. S1. The AMS detector showing the main elements and their functions. AMS is a TeV precision, multipurpose particle physics magnetic spectrometer in space. It identifies particles and nuclei by their charge  $Z$ , energy  $E$  and momentum  $p$  or rigidity ( $R = p/Z$ ), which are measured independently by the Tracker, TOF, RICH and ECAL. The ACC counters, located in the magnet bore, are used to reject particles entering AMS from the side. The AMS coordinate system is also shown. The  $x$  axis is parallel to the main component of the magnetic field and the  $z$  axis is pointing vertically with  $z = 0$  at the center of the magnet.

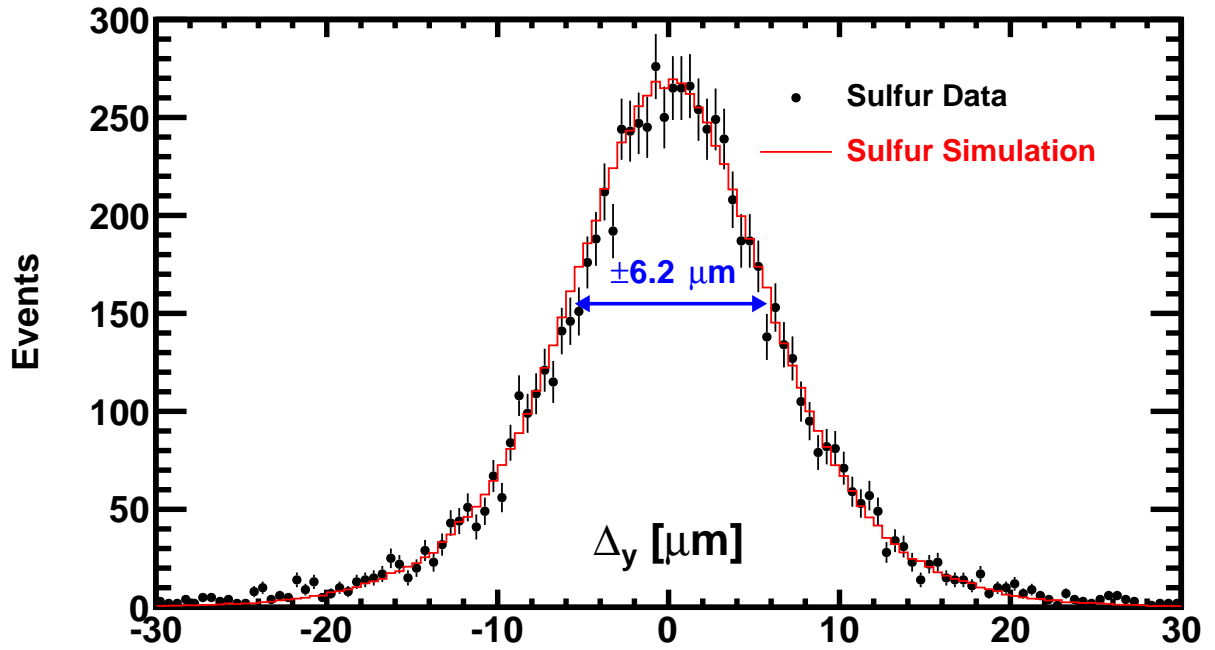


FIG. S2. Comparison of the differences of the coordinates measured in  $L3$  or  $L5$  to those obtained from the track fit using the measurements from  $L1$ ,  $L2$ ,  $L4$ ,  $L6$ ,  $L7$ , and  $L8$  between data and Monte Carlo simulation in the rigidity range  $R > 50$  GV for sulfur nuclei. The observed bending coordinate accuracy is  $6.2 \mu\text{m}$ .



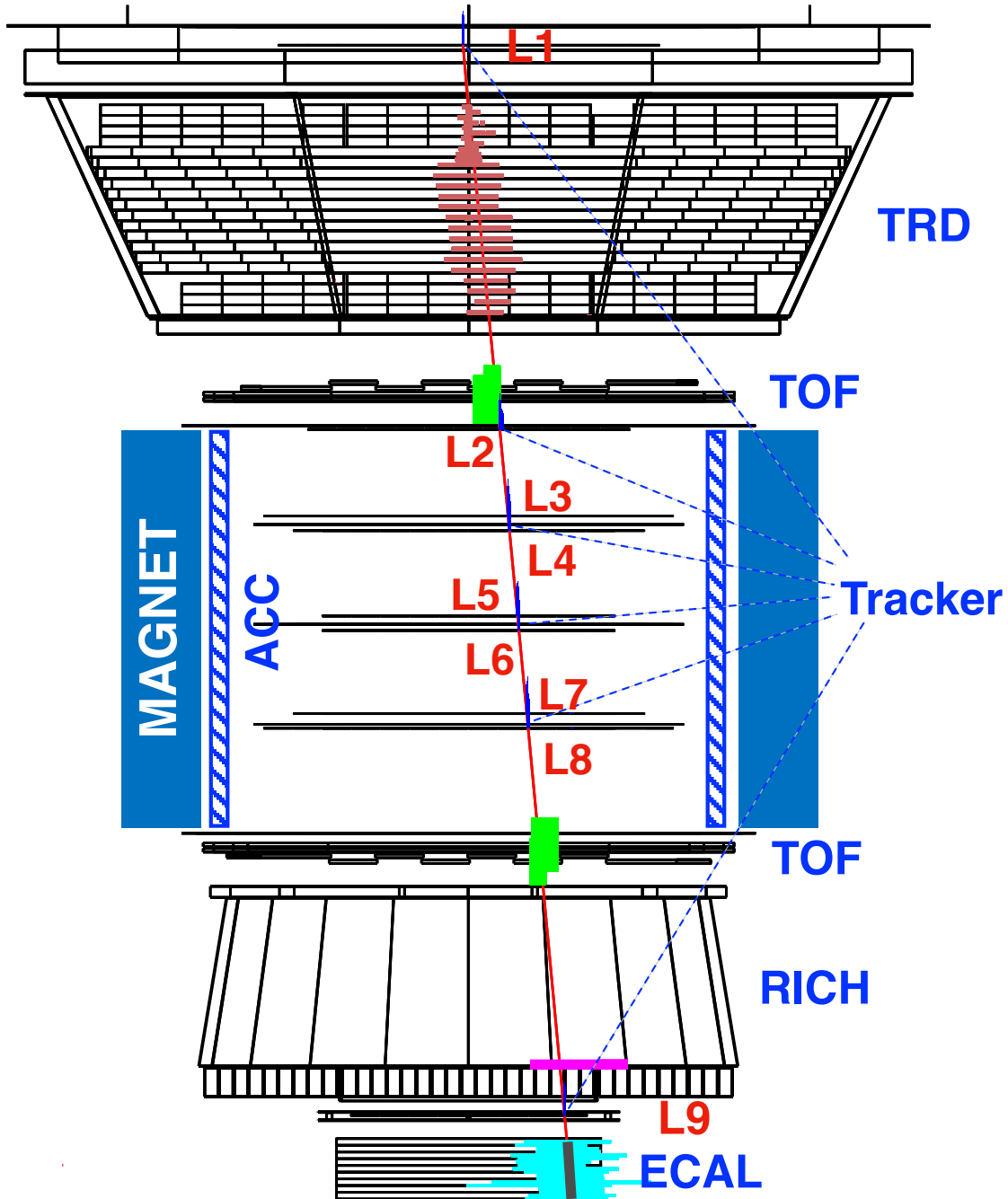


FIG. S3. A display of a sulfur nucleus event in the bending plane. The red line indicates the reconstructed trajectory. The dark red spread in TRD shows the  $dE/dx$  measurements in different TRD layers, green areas in upper and lower TOF carry the information of the  $dE/dx$  as well as the coordinate and time measurements. The vertical blue lines in the tracker layers carry the information of coordinates and  $dE/dx$  or pulse heights. The magenta line in RICH shows the reconstructed Čerenkov photons ring, the light blue area in ECAL shows the shower development and the black rectangle indicates the shower axis. This downward-going event is identified as a sulfur nucleus ( $Z=16$ ) with  $R = 27$  GV.

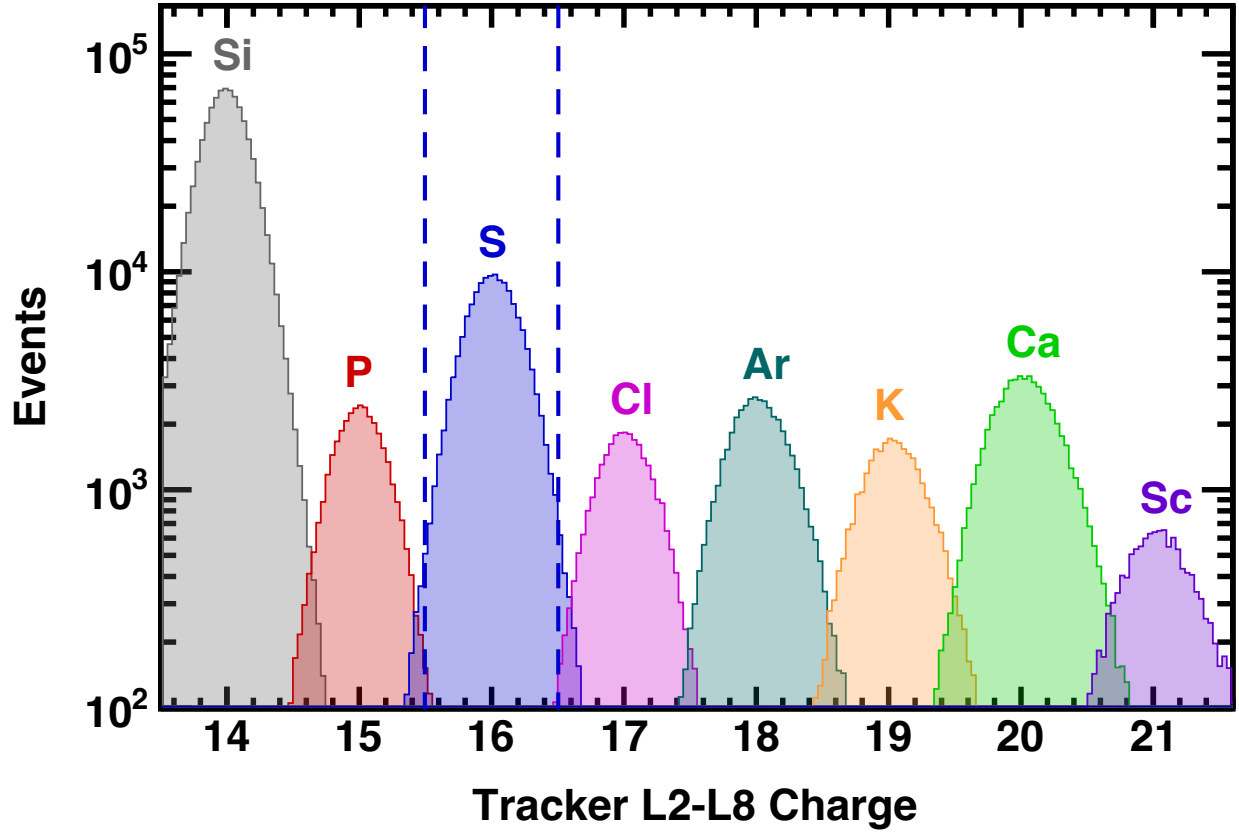


FIG. S4. Distribution of the charge measured with the inner tracker  $L2-L8$  for samples from  $Z = 14$  to  $Z = 21$  selected by the combined charge measured with  $L1$ , the upper TOF, and the lower TOF for rigidities above 4 GV. The dashed vertical lines correspond to the charge selection in the inner tracker for sulfur.

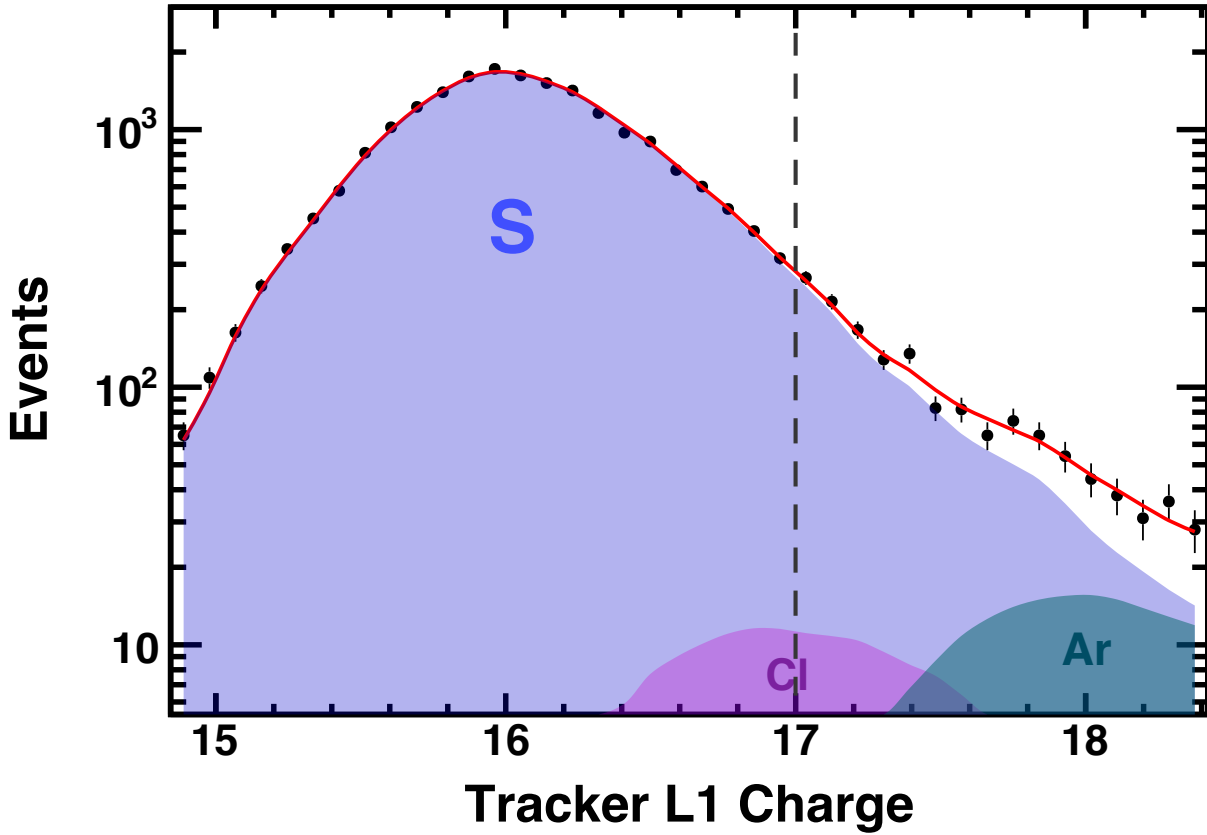


FIG. S5. Charge distribution measured by tracker  $L1$  for sulfur events selected by the inner tracker  $L2-L8$  in the rigidity range between 18 and 22 GV (black dots). The solid red curve shows the fit to the data of the sum of S, Cl, and Ar charge distribution templates. The charge distribution templates are obtained from a selection of non-interacting samples at  $L2$  by requiring that  $L1$ , upper TOF, and  $L3-L8$  measure the same charge value. The charge selection applied on tracker  $L1$  for sulfur is shown as a vertical dashed line.

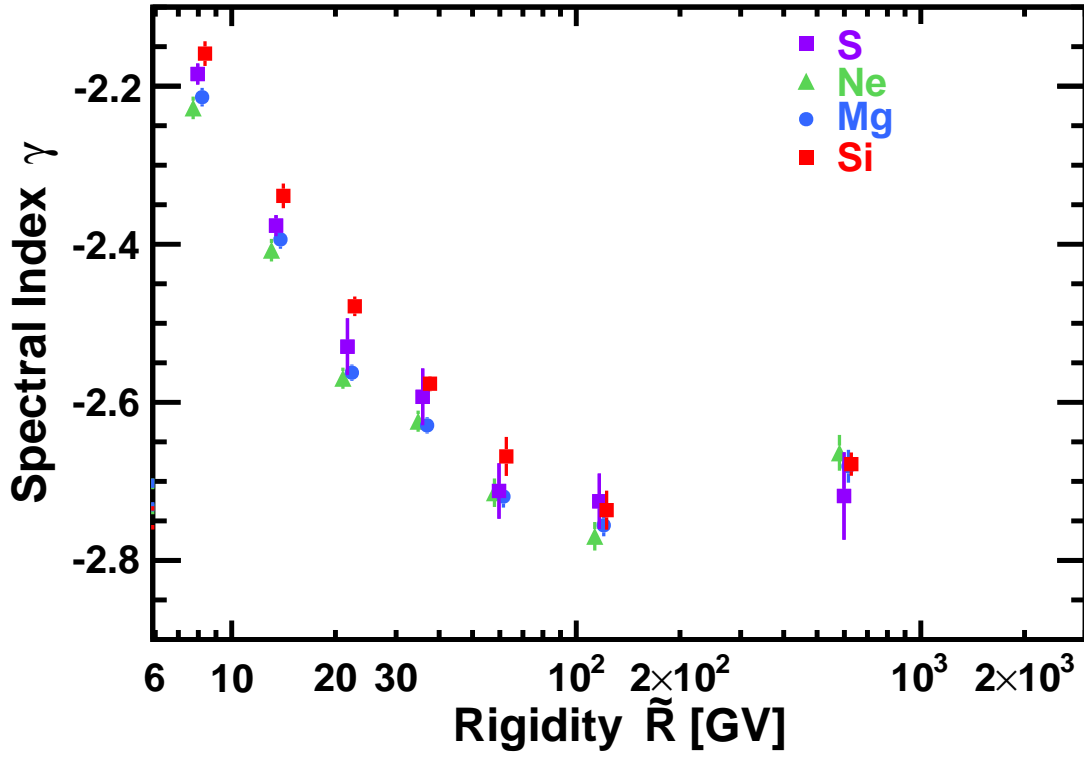


FIG. S6. The rigidity dependence of the S, Ne, Mg, and Si spectral indices. As seen, in the rigidity range 5.9 to 80.5 GV, the Ne, Mg, and S spectral indices are all lower than Si spectral index, and the spectral indices of four elements are identical above  $\sim 80$  GV. For clarity, the Ne, Mg, and Si data points are displaced horizontally.

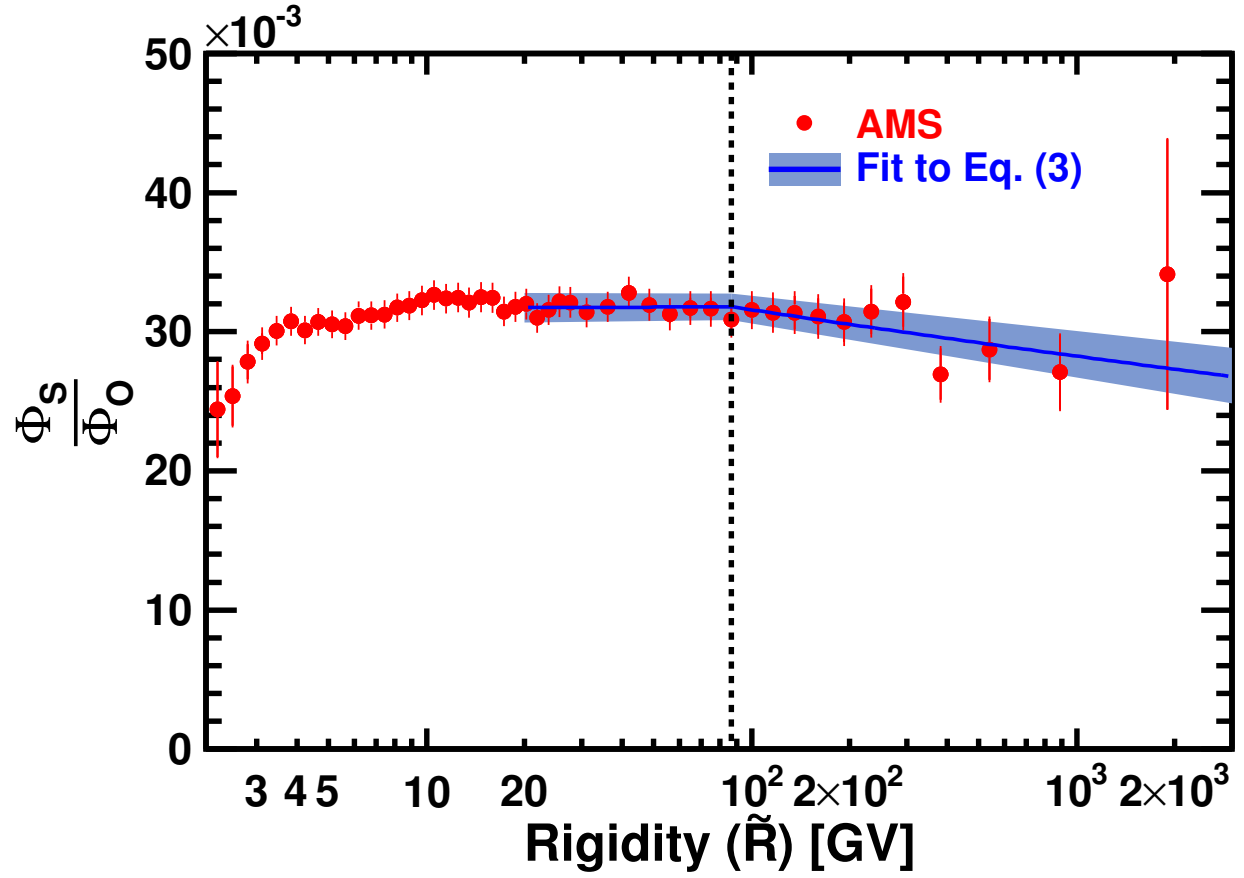


FIG. S7. The AMS  $\Phi_S/\Phi_O$  with total errors as function of rigidity together with the fit to Eq. (3) above 20 GV. The fit yields  $C = 0.032 \pm 0.001$ ,  $\Delta = 0.001 \pm 0.010$ ,  $\delta = -0.05 \pm 0.02$  with a  $\chi^2/\text{d.o.f.} = 15/22$ . The solid blue curve shows the fit result, blue area shows the fit total error ( $1\sigma$ ), and the vertical dashed line separates two fit intervals of Eq. (3).

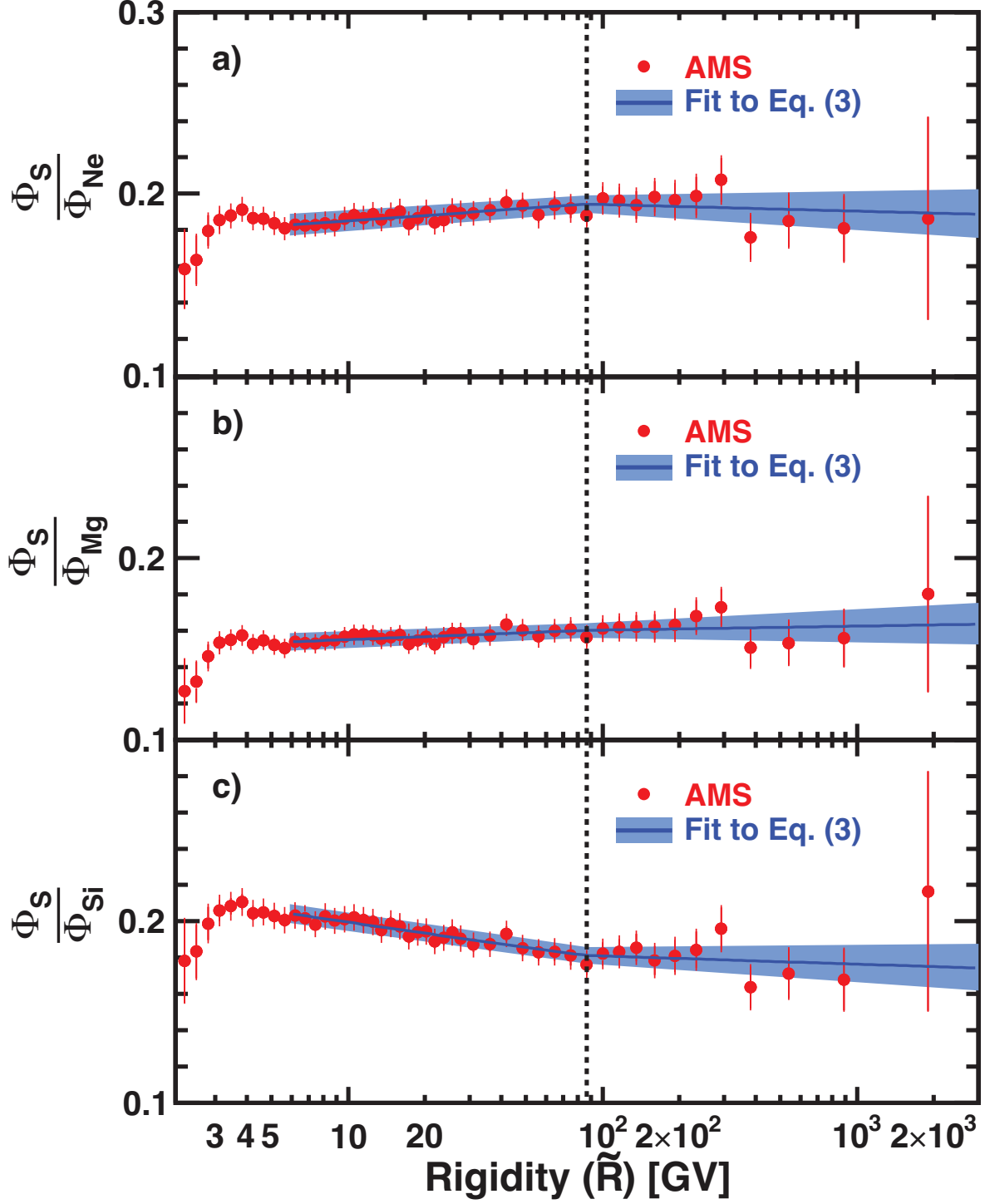


FIG. S8. The AMS a)  $\Phi_S/\Phi_{\text{Ne}}$ , b)  $\Phi_S/\Phi_{\text{Mg}}$ , and c)  $\Phi_S/\Phi_{\text{Si}}$  with their total errors as functions of rigidity together with the fits to Eq. (3). The solid curves show the fit results, blue areas show the fit total errors ( $1\sigma$ ), and the vertical dashed lines separates two fit intervals of Eq. (3). For  $\Phi_S/\Phi_{\text{Ne}}$ , the fit yields  $C^{S/\text{Ne}} = 0.194 \pm 0.004$ ,  $\Delta^{S/\text{Ne}} = 0.022 \pm 0.007$ , and  $\delta^{S/\text{Ne}} = -0.008 \pm 0.019$  with a  $\chi^2/\text{d.o.f.} = 21/36$ . For  $\Phi_S/\Phi_{\text{Mg}}$ , the fit yields  $C^{S/\text{Mg}} = 0.160 \pm 0.004$ ,  $\Delta^{S/\text{Mg}} = 0.015 \pm 0.006$ , and  $\delta^{S/\text{Mg}} = 0.006 \pm 0.019$  with a  $\chi^2/\text{d.o.f.} = 20/36$ . For  $\Phi_S/\Phi_{\text{Si}}$ , the fit yields  $C^{S/\text{Si}} = 0.181 \pm 0.005$ ,  $\Delta^{S/\text{Si}} = -0.045 \pm 0.006$ , and  $\delta^{S/\text{Si}} = -0.011 \pm 0.020$  with a  $\chi^2/\text{d.o.f.} = 19/36$ .

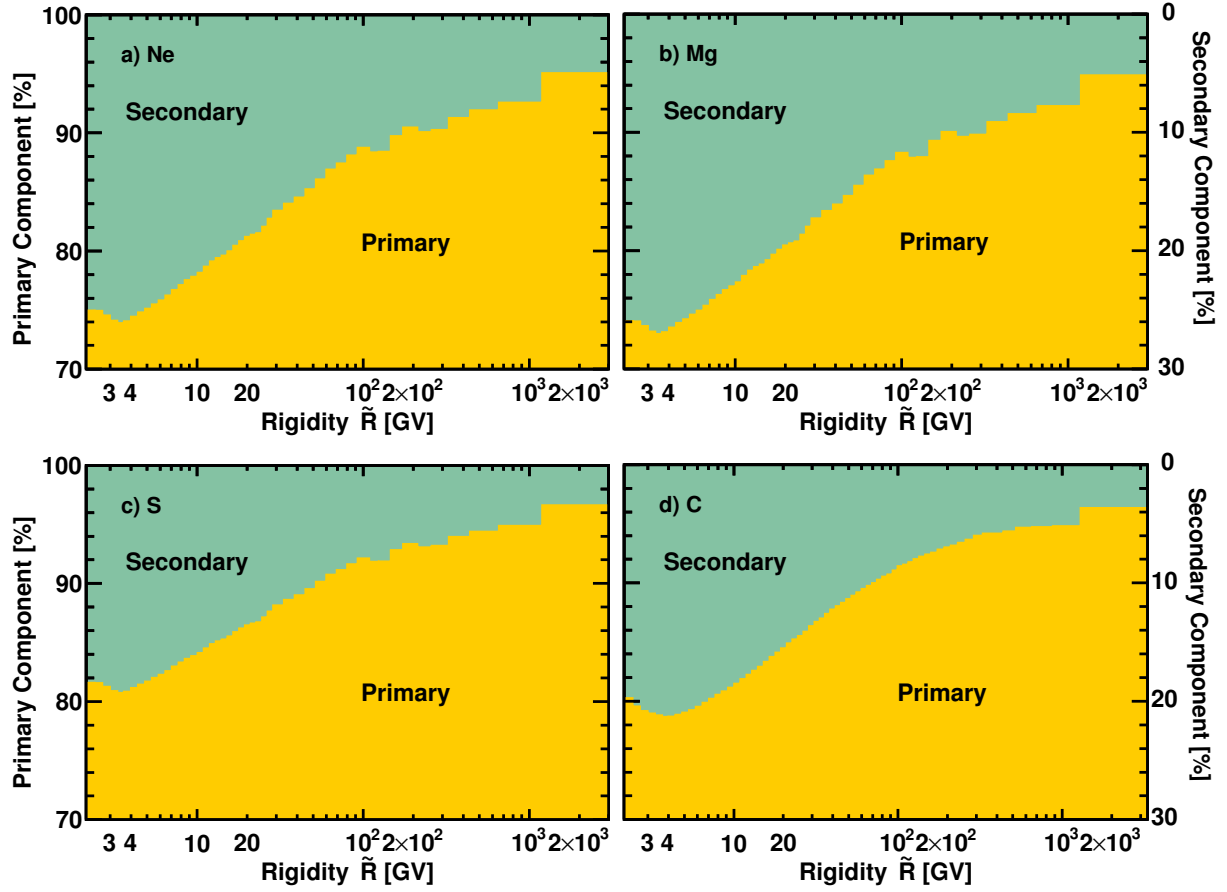


FIG. S9. The fractions of the primary and secondary components in a) Ne, b) Mg, c) S, and d) C fluxes in % as functions of rigidity, obtained from Fig. 4. As seen, above  $\sim 4$  GV, with increasing rigidity, the contributions of the primary component increase for all fluxes.